

ACP Mooringe Pty Ltd

Plympton

Residential DPA

TRAFFIC ASSESSMENT REPORT Project No. 190190 Doc No. WGA190190-RP-TT-0001 Rev. C

30 October 2019



Revision History

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1.1 BACKGROUND

Wallbridge Gilbert Aztec (WGA) has been engaged to undertake a Traffic Assessment for proposed Rezoning in Plympton, SA.

A locality plan of the proposed rezoning is illustrated by the area shaded red, in Figure 1.



Figure 1: Proposed Land Rezoning, Locality Plan

1.2 PURPOSE OF THE ASSESSMENT

The purpose of this report is to provide analysis of the existing and proposed future traffic impacts that will be utilised to determine requirements and what they may be, for the proposed rezoning.

The purpose and key elements of the study are to review and assess:

- Existing traffic flow conditions on the roads adjacent to the site;
- Background traffic conditions and any programmed roadway improvements;
- The traffic impact of the proposed rezoning on the adjacent road network;
- The suitability of the access points and internal road layout for the Rezoning, and;
- Vehicle capacity, road safety, and / or traffic operational constraints for the proposal, as well as potential measures to mitigate such constraints, where appropriate.

The methodology used in this analysis has been based on the City of West Torrens Development Plan (CWTDP), City of West Torrens Transport Strategy (2009), relevant Australian Standards and Austroads guidelines.

PROPOSED DEVELOPMENT

The Rezoning scenario is for future residential use of the land (medium density, low rise development). Approximately 2300 square metres of new internal road network is proposed for the Rezoning, with three access points onto surrounding the local network.

The site is bounded to the north by Mooringe Avenue, to the south by Gardener Street and the west by Streeters Road, with existing development to the east of the Rezoning site. The proposed road layout of the Rezoning is shown in figure 2 – however note that the layout is only preliminary and may change during the Development Planning phase of the design and approvals process.

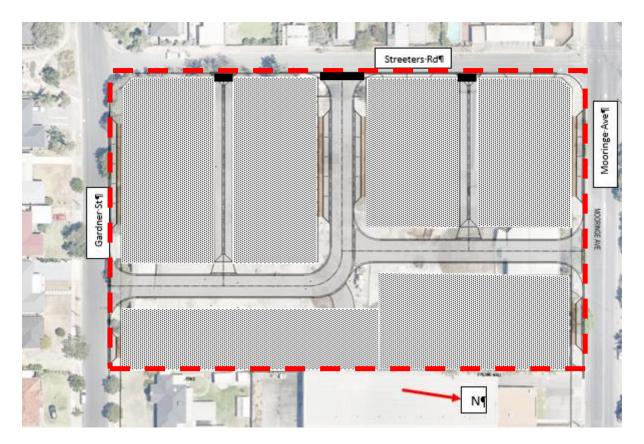


Figure 2: Proposed Rezoning Road Layout

D EXISTING ROADWAY AND TRAFFIC CONDITIONS

3.1 EXISTING CONDITIONS

Currently the site is zoned industry land use. It has previously been used as a transport depot with warehousing and offices, and at the time of the preparation of this report the site was undergoing demolition and remediation. The proposed medium-density residential redevelopment will require rezoning of the current land use. Figure 1 indicates locations of the local road network and Figure 3 indicates the location of arterial and sub arterial connections to Mooringe Avenue in relation to the Rezoning.

3.1.1 Mooringe Avenue

Mooringe Avenue abuts the Rezoning site on the northern side and is anticipated to cater for the majority of trips to and from the Rezoning, either directly or through the adjoining local network.

The road comes under the care and control of City of West Torrens and they have defined the road hierarchy as an Urban Local Road – Major Collector in their Transport Strategy (2009). The road is also specified as a Primary Freight Route on Council's road network and frequently has general access and sometimes has restricted access vehicles using it to access the industrial areas of Camden Park and North Plympton. From our review we agree that the role and function of Mooringe Avenue aligns with a Major Collector road

Mooringe Avenue is a single lane in each direction with restricted parking both sides of the road. The road width is approximately 12m kerb to kerb. The road reserve has footpaths and mature street trees. A part time bike lane is marked east of Errington Street. The southern (westbound) side of Mooringe Avenue is operational between 8-9am on school days and the northern (eastbound) side is operational 3-4pm on school days.

Mooringe Avenue adjoins Marion Road to the east and Morphett Road to the west. Mooringe Avenue is approximately 1.6km in length, and the Rezoning site is roughly at the midpoint of Mooringe Avenue, IE 800m west of Marion Road, 800m east of Morphett Road.

A pedestrian actuated crossing (PAC) is located on Mooringe Avenue between Streeters Road and Errington Street. When the PAC is activated it assists traffic to egress Streeters Road onto Mooringe Avenue and would also assist to platoon traffic to improve gap acceptance for egress of traffic from other side roads (EG Streeters Road, Whelan Avenue) onto Mooringe Avenue.

Based on existing available data obtained from DPTI supplied counts near the Marion Road intersection, the Average Annual Daily Traffic (AADT) volumes are in the order of 10,500 VPD, with approximately 10 percent comprising of heavy vehicle traffic. AM peak hour is between 7.45 - 8.45 and PM peak hour is between 4.45 - 5.45pm. A recent turning count supports DPTI's supplied counts. The posted speed limit is 60 kph.

3.1.2 Marion Road

Marion Road connects to Mooringe Avenue at the eastern end via a signalised intersection and is anticipated to cater for the majority of trips to and from the Rezoning due to its proximity to the broader arterial road network, connectivity to the southern and northern major arterials, links to inner western Adelaide and the Adelaide CBD. Marion Road is a two-way four lane divided arterial road that falls under the care, control and management of DPTI.

Based on existing available data obtained from DPTI supplied counts the Average Annual Daily Traffic (AADT) volumes are 33,500 VPD, with approximately 5.8 percent comprising of heavy vehicle traffic. The posted speed limit is 60 kph. Turning Counts for the signalised intersection is attached to Appendix B.

3.1.3 Morphett Road

Morphett Road connects to Mooringe Avenue at the western end via an uncontrolled at grade intersection and is anticipated to cater for a smaller proportion of trips to and from the Rezoning as it is in an anti-directional position to the Adelaide CBD, but may provide reasonably direct access to shops, schools, recreational facilities and the beach. Morphett Road is a single lane in both directions. Morphett Road falls under the care and control of West Torrens Council. The posted speed limit is 60km/h. Volumes are unknown at the intersection, as a comparison AADT is 12,600 VPD with 5.5% CV south of Anzac Highway, however traffic volumes drop substantially north of Anzac Highway as the road no longer serves an arterial purpose.

3.1.4 Streeters Road

Streeters Road abuts the Rezoning site on the western side and may cater for a small proportion of trips to and from the Rezoning. The road comes under the care and control of West Torrens Council and they have defined the road hierarchy as an Urban Local Road – Local Collector in their Transport Strategy (2009) – although this only applies to Streeters Road north of Mooringe Avenue, with Whelan Road providing the continuation of the Local Collector role to the south of Mooringe Avenue.

Streeters Road south of Mooringe Avenue would be classified as an Urban Local Road – Local Street. Council has expressed a desire to limit access to the rezoning from Streeters Road adjacent to the development.

Streeters Road consists of a single lane in each direction and has street lighting on dedicated poles. Residential property is located on the west side of Streeters Road, with access provided to existing residential allotments via the road. Streeters Road has a narrow road width and verge width from the back of kerb to the site boundary and that this would need further investigation into widening, potentially acquiring land from the site to both facilitate the development and have an active interface to the street. Any potential acquisition required for road widening purposes could be dealt with during the land division stage.

The road width is approximately 6m kerb to kerb, so available on-street parking is very limited. The new development will likely require parking bans along the length of road unless indented parking is provided (requiring transfer of land to road verge). Before the site was demolished, some parking had been created within private land at the northern end of the road, where the new development is proposed to have frontage. The road reserve on the western side has footpaths and lighting, however the eastern side of the road has undergone demolition with currently no street furniture or infrastructure (construction safety fencing borders the kerbing). Streeters Road forms a 4-way intersection with Mooringe Avenue and utilises a give way treatment to reinforce Mooringe Ave as the priority road. Streeters Road forms a junction with Gardner Street and does not have traffic control measures.

Traffic data was not supplied for this road, however, a turning count confirms that the Streeters Road leg north of Mooringe Avenue, carriers substantially more traffic than the southern leg (which has very low traffic volumes). Recorded volumes are discussed further in Section 3.5. The speed limit is 50 kph.

3.1.5 Gardner Street

Gardner Street abuts the Rezoning site on the southern side and is anticipated to cater for a reasonable proportion of trips to and from the Rezoning, when considering a suitable access point to the local road network generally. The road comes under the care and control of City of West Torrens and they have defined the road hierarchy as an Urban Local Road – Local Street in their Transport Strategy (2009).

Gardner Street is a single lane in each direction and has street lighting mounted on SAPN poles. The road width is approximately 9m kerb to kerb, so street parking is currently available both sides of road. The road reserve has footpaths and mature street trees. Gardner Street adjoins/intersects Streeters Road, Errington Street and Whelan Street (roundabout).

Traffic data was not supplied for this road, however, on site observations at 5:45pm on a typical weekday indicated only low volumes adjacent to the Rezoning (approximately 100 Veh/Hr). The posted speed limit is 50 kph.

3.1.6 Errington Street

Errington Street is located to the east of the Rezoning site and is anticipated to cater for a reasonable proportion of trips to and from the Rezoning, via Gardner Street. The road comes under the care and control of West Torrens Council and they have defined the road hierarchy as an Urban Local Road – Local Street in their Transport Strategy (2009).

Errington Street is a single lane in each direction and has street lighting on dedicated poles. The road width is approximately 9m kerb to kerb and has on street parking. A part time bike lane is marked and operational between 8-9am on school days for the southbound direction and 3-4pm on school days for the northbound direction. Plympton International College is located on Errington Street to the south of the proposed rezoning. The road reserve has footpaths and mature street trees.

Errington Street forms a 4-way intersection with Mooringe Avenue and utilises a give way treatment to reinforce Mooringe Ave as the priority road. Errington Street forms a 4-way intersection with Gardner Street with give way priority to Errington Street (Gardner Street has give way treatment).

Traffic Data was not supplied for this road, however, based on the adjacent land uses we anticipate traffic volumes in the order of 2000 VPD. The posted speed limit is 50 kph.

3.1.7 Whelan Avenue

Whelan Ave is located to the west of the Rezoning site, running parallel to Streeters Road. The road comes under the care and control of West Torrens Council and they have defined the road hierarchy as an Urban Local Road – Local Collector in their Transport Strategy (2009).

Whelan Avenue is a single lane in each direction and has street lighting on SAPN poles. The road width is approximately 9m kerb to kerb and has temporary on street parking outside the hours of 9-10am and 2-3pm Monday to Friday, when a no standing zone takes effect (both sides of road). The road reserve has footpaths and mature street trees. Whelan Avenue adjoins Mooringe Avenue and is controlled by a give way treatment. Whelan Avenue also forms an intersection with Gardner Road and is controlled by a roundabout.

Whelan Avenue is anticipated to cater for a reasonable proportion of trips to and from the Rezoning, considering that the junction with Mooringe Avenue (rather than intersections for example at Errington

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Street and Streeters Road) and roundabout at Gardner Street, may attract traffic due to perceived convenience by some road users.

Based on existing available data from the City of West Torrens Transport Strategy (2009), the Average Annual Daily Traffic (AADT) volumes for this road are in the order of 3000 VPD, with only a low percent comprising of heavy vehicle traffic. The posted speed limit is 50 kph.



Figure 3: General Arterial and Sub Arterial Road network layout

3.2 ROAD CRASH HISTORY

DPTI provides road crash data via Location SA Map Viewer from 2013 to 2017 (5 year crash history). Figure 4 shows the locations of recorded crashes(circled in red) in the vicinity of the Rezoning site.

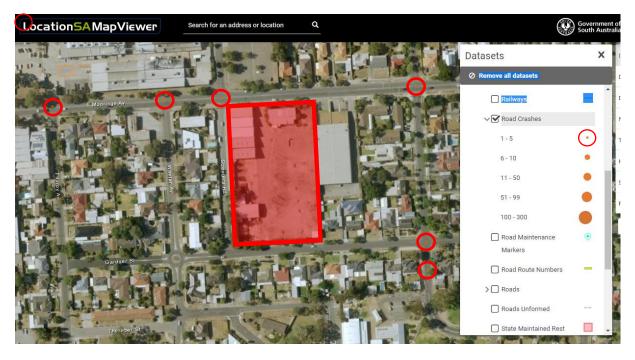


Figure 4: Location of crash(es) indicated by orange dots on plan around the highlighted development.

The local crash data is summarised below in Table 1. Only intersections with crash history between 2013-2017 are represented in the table, and separated into Serious Injury (requires hospitalisation), Injury (report of an injury usually accompanying review by doctor), and Property Damage Only (PDO). The major junctions at either end of Mooringe Ave are also considered.

Mooringe Ave / Streeters Rd					
Crash Type	Serious Injury	Injury	PDO		
Right Angle	1 (25%)	2 (50%)	1 (25%)		
TOTAL		4			
	Mooringe Ave	/ Errington St			
Crash Type	Serious Injury	Injury	PDO		
Right Angle	0	0	1 (50%)		
Hit Pedestrian	0	1 (50%)	0		
TOTAL		2			
	Mooringe Ave	e / Marion Rd			
Crash Type	Serious Injury	Injury	PDO		
ALL CRASHES	0	6	8		
Rear End	6 (42.9%)				
Hit Pedestrian	1 (7.1%)				
Right Turn	7 (50%)				
TOTAL 14					
	Gardner St /	Errington Rd			
Crash Type	Serious Injury	Injury	PDO		
Right Angle	0	0	1 (100%)		
TOTAL		1			
	Mooringe Ave	/ Whelan Ave			
Crash Type	Serious Injury	Injury	PDO		
Right Angle	0	0	2 (100%)		
TOTAL		2			
	Mooringe Ave	/ Morphett Rd			
Crash Type	Serious Injury	Injury	PDO		
All crashes	0	2	14		
Rear End		5 (31.25%)			
Hit Fixed Object		1 (6.25%)			
Side Swipe		1 (6.25%)			
Right Angle		7 (43.75%)			
Roll Over		1 (6.25%)			
Other		1 (6.25%)			
TOTAL	L 16 (100%)				

Table 1: Road Crash History (2013 - 2017) - various locations, Plympton area

In summary the intersections and junctions around the Rezoning site are performing as would be expected for at grade intersections formed between local network roads and a collector road. As shown in Figure 3, all crashes occur at "conflict points" in the network (junctions or intersections where opposing movements are undertaken) with the exception of one crash on Errington Street south of the Gardener Street Intersection. No existing Black Spot Sites (where greater than 5 injury crashes/5 years are recorded) were identified in the vicinity of the Rezoning site, with the exception of Marion Road and Mooringe Avenue (discussed below).

The crash history of the intersection of Mooringe Avenue and Streeters Road is worthy of consideration as the proposed development will likely increase traffic on the Streeters Road (South) by approximately 500 VPD (discussed later in Section 5 of this report) with the majority of these volumes expected to be turning right out of Streeters Road onto Mooringe Avenue. The current intersection records on average less than one crash per year, with the predominant crash type being right-angle crashes. The predominant crash type is relatively common for an "uncontrolled" 4-way intersection, and moderate traffic volumes on Mooringe Avenue. Whilst the proportion of injury crashes is high for an urban road (75%), the lower frequency of crashes indicate that the intersection is performing adequately. It is recommended that the layout of the proposed development and landscaping observe the SISD sight line requirements as defined in Figure 9 – Austroads Guide to Road Design Part 4A – "Figure 3.2".

The junctions either end of Mooringe Avenue have comparatively higher crash rate histories due to their larger volumes. The Marion Road arterial road junction is performing adequately, fundamentally due to the intersection being controlled by traffic signals, although it should be noted that the proportion of injury crashes is relatively high at 43%. The site is technically a Black Spot, and would be eligible for Black Spot funding, however the responsibility for determination of treatment options and application for funding lies with DPTI.

In terms of total crashes, the Morphett Road junction has the worst performance out of those assessed, although the proportion of injury crashes is much lower than Marion Rad. The higher incidence of crashes is largely due to volumes (intersection of two sub arterial roads) which means that gap acceptance thresholds are lower, and as it is uncontrolled (give way treatment) requiring judgement from individual drivers to pick gaps (correspondingly right-angle crashes have the statistically highest crash type). Signalising of this junction would assist with both crash reductions and clearing of queues on Mooringe Avenue – however this is not part of the Transport Strategy Report (2009) or a priority for West Torrens Council.

3.3 PLANNED ROADWAY IMPROVEMENTS

Existing road geometries are relatively fixed by adjoining development and are expected to remain the same. All junctions and intersections assessed do not have any obscure intersecting geometry, however sight line impediments (such as mature vegetation, SAPN poles and boundary fencing) exist when exiting side roads onto Mooringe Avenue. Council's Transport Strategy (2009) mentions minor widening of Streeters Road at Mooringe Avenue for left and right turn exit lanes – as discussed above, potential acquisition and land transfer to council verge could occur during the land division stage.

The report also mentions the proposed upgrade of Mooringe Avenue and Marion Road intersection to cater for B-double turning movements - the responsibility for this upgrade lies with DPTI and the timing of the upgrade is unknown. Linking of Richmond Road and Morphett Road is also mention in the Transport Strategy - if that were to occur some freight may bypass Mooringe Avenue as improved links east-west could be established to the adjacent industrial areas that are located next to the airport. The Overlay Map WeTo/1 – Transport, referred to in CWTDP is attached in the Appendix A, however there are no impacts from the overlay map that need to be considered in this Traffic Assessment Report.

The City of West Torrens is currently preparing a Local Area Traffic Management (LATM) Plan which is in Stage 2 consultation at the time this report was written, this site fits within the study area. However, the proposed LATM Plan found traffic conditions around the location of interest to be acceptable in comparison with the strategic transport plan criteria. Hence proposed LATM projects will likely not impact the Rezoning site.

3.4 EXISITING PEDESTRIAN AND CYCLIST INFRASTRUCTURE

The CWTDP indicates cycling routes (Bikedirect Network) in its overlay plans – refer Overlay Map WeTo/12 Transport in Appendix A. There are no designated "*Main Road – Bike Lane*" roads within the vicinity of the Rezoning, Mooringe Avenue is designated as a "*Secondary Road – Bike Lane*" (east of the Rezoning), as is Morphett Road.

There is an existing shared pedestrian and cyclist path that runs adjacent to Osborne Terrace, known as the Westside Bikeway – this is indicated as a "*Off Road Sealed Path*" in the Bikedirect Network. These cycling and walking (shared) facilities will likely attract patronage from the subsequent development for both recreational and commuting activities, as the path connects "off road" as far as Mile End north-easterly and Novar Gardens south-westerly. The local network would generally be used to access the Westside Bikeway via Gardner Street and Errington Street, alternatively Mooringe Avenue bike lanes connect to the Westside Bikeway at the Marion Road intersection. Other links include the footpath at the south end of Streeters Road connecting through to Myer Avenue.

As mentioned in section 3, both Mooringe Avenue and Errington Street have part time bike lanes, however they are relatively discontinuous and established to provide safer cycling links to the nearby Plympton International College.

Strava Heat Map can be used to represent cycling activity in the proximity of the proposed development - refer Figure 5. The white layer represents the highest level of cycling activity, darker blue layers indicates "moderate" cycling activity where purple is "lower" cycling volumes. It is evident that Mooringe Avenue, Morphett Road, Marion Road and the Westside Bikeway have relatively more cycling patronage than the surrounding local areas. Comparatively Cross Road, Anzac Highway and Marion Road attract much higher cycling activity.

The proposed internal road network of the development will be designed in accordance with AMCORD guideline for "Characteristics of Street Types", and Councils requirements, to cater for safe pedestrian movements and sharing the road with cyclists.

In summary, the Rezoning is relatively well connected to existing on road bicycle routes and networks that facilitate cycling.



Figure 5: Strava Heat Map indicating cycling activity

3.5 EXISITING PUBLIC TRANSPORT INFRASTRUCTURE

Bus route 167 & 168 services the Adelaide CBD and Glenelg from this location. Additional bus routes (EG J7, J8 servicing between Marion and West Lakes) - and school buses utilise Mooringe Avenue. Public transport infrastructure (bus stop 12) is located adjacent to Mooringe Avenue and the Rezoning, which is located mid-block on Mooringe Avenue between Streeters Road and Errington Street. The bus stops (12 both directions & 13 eastbound only) have shelters and are well placed to service the Rezoning. Refer to Figure 6 for bus routes in the proximity of the proposed rezoning.

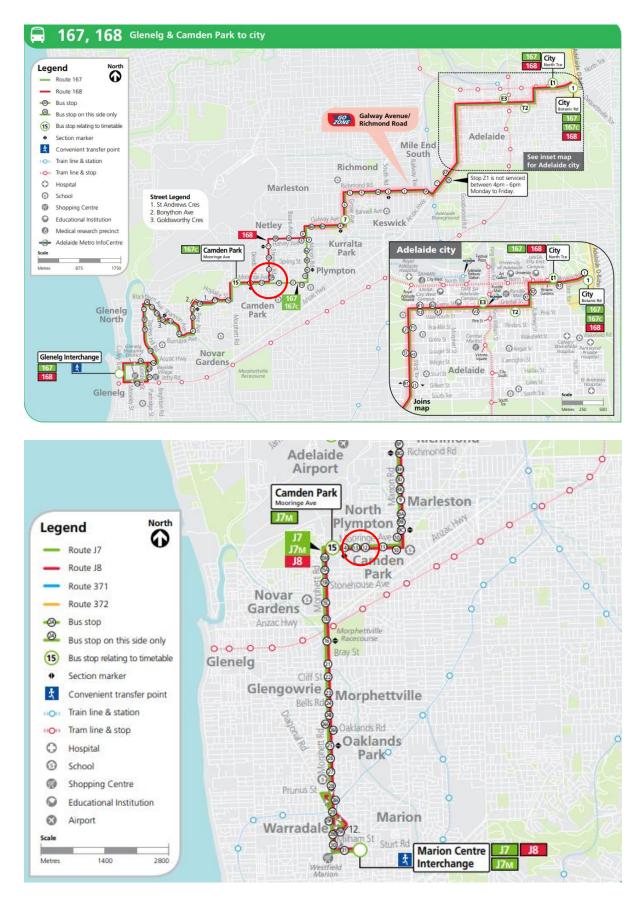


Figure 6: Bus routes in the proximity of The Rezoning

3.6 SITE SURVEY

A traffic survey of the existing 4-way intersection of Mooringe Avenue and Streeters Road was conducted on 3 April 2019, between 4:45pm and 5:45pm. This represented afternoon peak traffic during a typical weekday, coinciding with the peak hour determined from 11 hour counts conducted by DPTI on Marion Road / Mooringe Avenue Junction.

General observations were as follows:

- Weather fine, conditions clear and light (afternoon daylight saving).
- Traffic much heavier on Mooringe Avenue compared to Streeters Road.
- Traffic volumes much heavier on Streeters Road north leg, Streeters Road south leg had very low volumes.
- Relatively high right out / left in volumes on Streeters Road north leg.
- The "collector road" nature of Whelan Avenue, which terminates at Mooringe Avenue (northbound), appears to continue onto Streeters Road north leg.
- Around half a dozen cyclists were using Mooringe Avenue during the count (cyclist volume is not included in below counts).
- The remedial site work at the Rezoning site may have influenced some of the Streeters Road traffic behaviour, however the site works are not expected to be a large influence.

Table 2 represents the PM Peak hour turning count results. Figure 7 represents the recorded turn counts diagrammatically. Note that in Figure 7, where no movement recorded any volume, it is not represented on the diagram - for example there were no vehicles turning left into Streeters Road south leg during the hour of traffic survey.

Table 2: Peak Hour Site Survey Results

Road	Direction of	Intersection Behaviour			
Road	Travel	Straight	Left	Right	
Mooringe Avenue	East	334	40	0	
Mooringe Avenue	West	495	0	25	
Streeters Road	North	0	1	0	
Streeters Road	South	2	30	83	

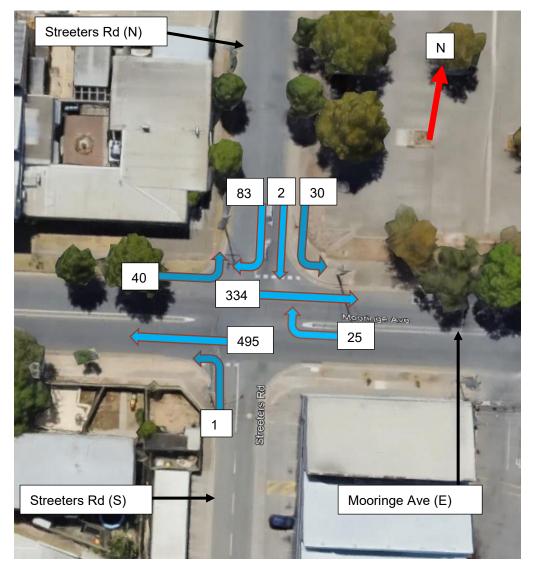


Figure 7: PM Peak Hour Site Survey Results

These results yield traffic volumes for a typical hour afternoon peak period. For the purpose of this investigation, these results are extrapolated to an hour peak period and a 10% ratio of peak hour to two-way AADT volumes is assumed. Based on this methodology, the site results yielded:

Mooringe Avenue:

- Weekday peak hour flow (two-way) = (334+495+40+25) = 894
- AADT (two-way) = 894 / 10% = 8,940
- The following commercial volumes were recorded on Mooringe Ave:
 - 12 Trucks and 4 busses westbound
 - 9 Trucks and 2 busses eastbound
 - Total Commercial Volume (CV) in peak hour = 27
 - Total CV % = 27 / 894 = 3%

Streeters Road (North Side):

- Weekday peak hour (two-way) = (2+30+83) = 115
- AADT (two-way) = 115 / 10% = 1,150
- The following commercial volumes were recorded on Mooringe Ave:
 - 2 busses (one left in, one right out)
 - Total Commercial Volume (CV) in peak hour = 2
 - Total CV % = 2 / 115 = 2%

Streeters Road (South Side):

- Weekday peak hour (two-way) = 1
- AADT (two-way) = 1 / 10% = 10
- No CV recorded on this side of Streeters Road.

The Mooringe Avenue AADT calculated from the site survey is similar to the AADT provided from DPTI (9,650 - 10,500). It is possible that Mooringe Avenue traffic volumes have reduced slightly from the early 2000's considering development is relatively established in the area already (little or no growth rate), and residents may have adopted a modal shift to alternative transport to commute to work (cycling, walking and public transport), car-pooling, and more flexible working hours allowing the commute outside of peak hour times.

In summary, during the PM traffic survey, the intersection operated relatively smoothly, with only the Streeters Road northern leg experiencing any reasonable delay due to waiting for breaks in traffic in both directions to turn right out. Mooringe Avenue flows without significant delays (sometimes right turning traffic into Streeters Roads will create a slowing of through traffic). Traffic on Mooringe Avenue (westbound) was generally travelling in platoons due to the upstream signals at Marion Road.

ROAD ACCESS NETWORK

4.1 STREET LAYOUT

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The proposed road network for the Rezoning is represented in Figure 8 and consists of a two-way through road access street (fronting and providing access to Mooringe Avenue (1) and Gardner Street (2)) and of which two cul-de-sac access lanes with stub ends branch off. Access lanes and cul-de-sacs have been designed to provide local access only to the Rezoning – however note that the layout is only preliminary and may change during the Development Planning phase of the design and approvals process. It is possible that "out only" access onto Streeters Road could be provided from the rezoning, but this is yet to be determined.

It is recommended these lanes will need to meet the specifications outlined in the City of West Torrens Requirements. The Access Street is to meet the AMCORD requirements for an Access Street (0-300 veh/day).

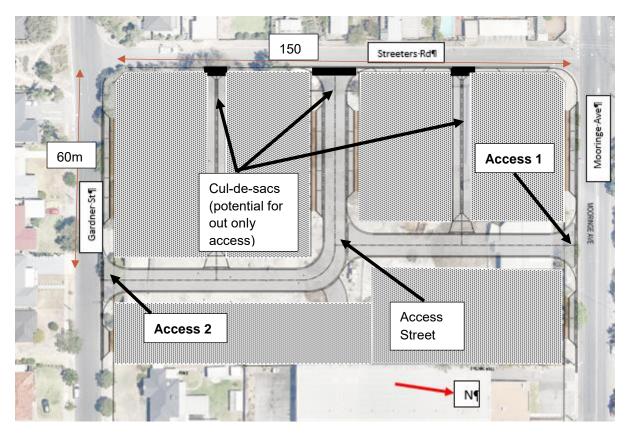


Figure 8: Internal Road Hierarchy

4.2 TRAFFIC MANAGEMENT AND ACCESS ARRANGEMENTS

The Rezoning internal road network will consider road geometry to assist in managing speed on the network and providing a safer environment.

Austroads Guide to Road Design Part 4A – Geometric Design (AGRD04A-17) table 7.2 "property access considerations on urban roads" states that: for local streets it is preferred that road networks are planned and designed so that property access points are located on local streets rather than arterial roads. Low travel speed and driver expectation of interference reduces the likelihood of conflict. Potential conflict with pedestrian movement must be identified and appropriate solutions adopted. However, the low speed environment should ensure that both the likelihood of conflict and the severity of crashes are minimised.

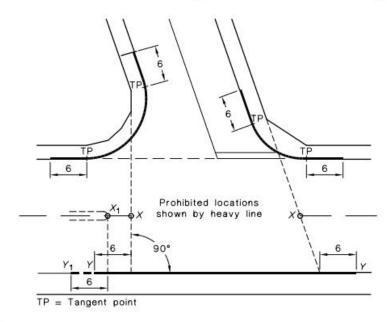
Four-way intersections have been avoided in order to minimise the likelihood of collisions. Austroads Guide to Road Design, Part 4A: Unsignalised and Signalised Intersections, states that unsignalised four-way intersections typically experience higher crash rates for the through movement from the minor road.

T-junctions (at right angles to the priority road) are favoured over four-way intersections and have been included at junctions between two local streets. A 90-degree intersecting angle provides the optimum sight line in both directions and the give way rule / priority is clear.

The following considerations must be made when detail designing the internal road layout for the Rezoning:

- Provide single manoeuvre turns by the design vehicle.
- Provide adequate clearance between the design vehicle's turning path and physical constraints within the property.
- Avoid reversing movements into or out of the Rezoning, except in the case of individual single residential houses.
- Provide adequate sight distance, including pedestrians (discussed further in section 4.4).
- Minimise pedestrian / vehicle conflict areas and control vehicle speed across footways.
- Access points will not be permitted within 6m of the tangent point of the curve as indicated in AS2890.1 *Parking Facilities* Figure 3.1 (refer below Figure 9). Consideration will need to be given to placement of the access points for corner allotments, and allotments where adjacent indented parking is proposed.

AS/NZS 2890.1:2004



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NOTES:

uaranteed when printed)

- Accesses to domestic driveways are excluded from the prohibition in respect of the kerb section marked Y-Y (see Clause 3.2.3(a)).
- 2 The points marked X_1 and X are respectively at the median end on a divided road and at the intersection of the main road centre-line and the extensions of the side road property lines shown as dotted lines, on an undivided road. On a divided road, dimension *Y*-*Y* extends to Point Y_1 .

DIMENSIONS IN METRES



Figure 9 – from AS2890.1 Parking Facilities

4.3 ON-STREET AND OFF-STREET PARKING

The City of West Torrens has determined that the rezoning will fit under Residential Medium Density Policy Area 18, and the parking requirement would be determined by PDC12 and 16, and Table WeT0/2.

PDC12 states that on-street vehicle parking should be provided at a ratio of **one car parking space for every two allotments**.

The City of West Torrens Development Plan (CWTDP), General Section, Land Division, Roads and Access (PDC16), indicates land divisions should provide space sufficient for on-street visitor car parking for the number and size of the allotments, taking account for:

- The size of proposed allotments and sites and opportunities for on-street parking
- The availability and frequency of public and community transport
- On-street parking demand likely to be generated by nearby uses.

CWTDP Table WeTo/2 indicates that 2 off-street car parking spaces are required per dwelling, one covered, one uncovered, refer to Figure 10 below.Assuming 82 dwellings for this development 164 car parking spaces are to be incorporated into the Rezoning, of which 82 are to be covered, 82 not required to be covered. There is potential for some of the uncovered parking spaces to be a combination of parking within driveways and on street parking, and this will need to be further investigated during the DPA phase.

West Torrens Council Table Section Table WeTo/2 - Off Street Vehicle Parking Requirements

Form of development		Number of Required Car Parking Spaces		
Accom	modation			
Dwellin	g	For detached, semi detached, row dwelling and multiple		
	detached	dwellings to provide:		
	semi-detached	2 car parking spaces per dwelling, one of which is		
	row	covered.		
	multiple	For group dwelling and residential flat building to provide:		
	group	2 car parking spaces per dwelling, one of which is covered		
	within a residential flat building	+ an additional 0.25 car parking spaces per dwelling.		

Figure 10: Table WeTo/2 Car Parking Spaces Requirement.

4.4 SIGHT DISTANCES

Austroads Guide to Road Design Part 4A – Geometric Design (AGRD04A-17) sets out requirements for minimum sight distances for intersections in Section 3. All intersections must achieve minimum approach sight distances (ASD), safe intersection sight distances (SISD) and minimum gap sight distances (MGSD). The internal junctions and new access points are shown in Figure 7 and SISD diagrammatic representation in figure 11.

The internal road network has not been assessed as part of this report, this relates to the ASD component of the analysis, which will be reviewed during the Rezoning Application Process. The proposed access points onto Streeters Road and Gardner Avenue will be assessed against the existing roads' theoretical speeds. The following parameters were adopted for sight distance calculations:

- Reaction Time, R_T = 2.0 sec (note D_T = R_T + 3.0 seconds)
- Coefficient of deceleration, d = 0.36
- Critical Acceptance Time, ta = 5 sec
- Longitudinal grade, a = 0%



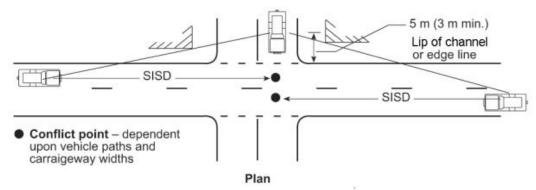


Figure 11: Austroads GTRDP4A "Figure 3.2"

4.4.1 Access Point One

Access Point One (AP1) is proposed to front Mooringe Avenue, between the two driveways of the former industrial site, 55m east of Streeters Road. Mooringe Avenue has a posted speed limit of 60 kph, this is thought to be a reasonable 85th percentile speed to adopt. The following minimum sight distances required of AP1 are:

- ASD AP1 = Not Reviewed
- SISD AP1 East and Westbound = V X D_T / 3.6 + V² / (254 X 0.36)

= 60 X (2+3) / 3.6 + 60² / (254 X 0.36) = 123m (in excess of 200m available both directions)

• MGSD AP1 = 83m (east and westbound) (from Table 3.6 AGRD04A-17)

All of these minimum sight distance requirements are achieved. A photo of Mooringe Ave adjacent to the Rezoning is shown in Figure 12.



Figure 12: Mooringe Avenue at the Streeters Road Intersection, looking easterly.

4.4.2 Access Point Two

Gardner Ave has a specified speed limit of 50 kph, this is thought to be a reasonable 85th % speed to adopt. The following minimum sight distances required of AP2 are:

- ASD AP2 = Not Reviewed
- SISD AP2 = 50X(2+3)/3.6+50²/(254X0.36) = 96.8m (>100m available)
- MGSD AP2 = 69m (from Table 3.6 AGRD04A-17) (>100m available)

All sight distances requirements are achieved. A photo of Gardner Ave adjacent to the Rezoning is shown in Figure 13.



Figure 13: Gardner Street at the south eastern corner of the Rezoning looking westerly.

4.5 SUSTAINABLE TRANSPORT INFRASTRUCTURE

Sustainable transport infrastructure for pedestrians and cyclists will be provided as part of the proposed Rezoning. This is to be consistent with details of the proposed are provided below.

4.5.1 Pedestrian and Cyclist Infrastructure

The WTCDP suggests developments should provide a permeable street and path network that encourages walking and cycling through the provision of safe, convenient and attractive routes with connections to adjoining streets, paths, open spaces, schools, pedestrian crossing points on arterial roads, public community transport centres and activity centres.

Linkage to the existing Westside Bikeway shared pedestrian and cyclist path is provided through the established local road and footpath network, which is considered sufficient to cater for the expected levels of patronage.

4.5.2 Public Transport Infrastructure

The CPDP requires new developments to be integrated with existing public transport corridors. The Rezoning is relatively well serviced with existing route services and the Rezoning located midway between bus stops 12 and 13 located on Mooringe Avenue (either of these bus stops are approximately 100m from the Rezoning). Tram Stop 10 is located approximately 1km south east from the Rezoning site and could be utilised as an alternative form of public transport with an excellent frequency of services, possibly in combination with cycling or "park and ride" transport options.

O TRAFFIC GENERATION AND DISTRIBUTION

5.1 TRIP GENERATION AND PEAK PERIOD

Adopted traffic generation rates for the proposed Rezoning have been based on the "Residential – House", and 'Residential – Medium Density Flats' contained within the RMS Guide to Traffic Generating Developments Version 2.2. They are shown in Table 3 below along with the estimated number of trips to be generated by the proposed Rezoning.

There are 82 dwellings proposed, nominated as 'Medium Density' - these have been assumed to be townhouses. The generation rates for townhouses are assumed the same as houses, and the apartment trip generation rates are assumed to fall under 'Medium Density Residential Flat Building – larger units and townhouses (three or more bedrooms)". The guideline provides a range of rates, for the purposes of sensitivity testing. The analysis will utilise the higher of the rates (in bold) which are considered to be a conservative representation of the Rezoning proposal.

		Daily Trips		Weekday Peak Ho	ur
Land Use	Estimated Number of Dwellings	Rate/Dwelling Trips I		Rate/Dwelling	Trips
Townhouses	82	5.0 (minimum) 6.5 (maximum)	410 533	0.5 (minimum) 0.65 (maximum)	41 54

Table 3: Proposed Development Traffic Generation

The use of the term 'trip' represents a one-way vehicular movement from one point to another but excluding the return journey. Therefore, a vehicle entering and leaving the Rezoning corresponds to two trips. The proposed Rezoning is expected to generate a total of 533 trips on a daily basis and approximately 54 trips during a weekday peak hour.

5.2 SPATIAL DISTRIBUTION OF TRIPS

The spatial distributions of traffic generated by the Rezoning/Site can be discussed separately as internal distribution within the site and the utilisation of each access point, and external distribution i.e. the interaction of traffic flow with the wider road network.

5.2.1 External Distribution

Trips generated by the Rezoning have been assumed to be distributed in two general directions – the CBD to the East via Marion Road and Glenelg to the West via Morphett Road. The assumed proportion of trips to each of these directions is shown in Figure 14 below.

It is assumed the CBD will attract majority of peak hour traffic due to the morning and evening commute for workers in the Rezoning. Local schools and the closest shopping centre are located both east (EG Kurralta Central, Hilton Plaza, Richmond Village) and west (Harbour Town, Glenelg) of the Rezoning. For the modelling it has been assumed that 85% of trips will be eastbound and 15% of trips will be westbound, which is considered to be a conservative approach for the traffic modelling that will intensify the volume of right turning vehicles out of Streeters Road South.



Figure 14: Spatial Distribution of Trips (External)

5.2.2 Internal Distribution

The Rezoning is proposed to accommodate three Access Points (APs) – discussed in Section 4.1. It is assumed that traffic within the site will opt for the closest AP by driving distance when arriving/exiting the site and make their way onto Mooringe Ave in the shortest distance possible. For the sake of modelling all trips are assumed to access the Rezoning via Streeters Road onto Mooringe Avenue, however in reality a proportion of trips will likely distribute to other parts of the local network IE Errington Street and Whelan Street via Gardner Street. In consideration of the above and also that the traffic from the industrial facility that was previously in operation at this location has not been discounted from the proposed new volumes, these modelling assumptions will result in a conservative traffic analysis.

5.3 PEAK PERIOD TRIP DISTRIBUTION

The resultant number of trips expected to be generated per AP is summarised in Table 4 based on the internal distribution of traffic and the amount of traffic generated at the north and south sides of the Rezoning.

The number of incoming/outgoing trips have been calculated based on the assumption that for residential lots in the Morning Peak, 90% of trips will be leaving the Rezoning with 10% entering the Rezoning and these ratios reversed in the Afternoon Peak Hour (this is considered to be a highly conservative estimation).

The following access point traffic proportions are assumed, based on rough area of dwellings on the site:

- AP1: 75% IE 75% of the total development will access / egress from this point;
- AP2: 25% IE 25% of the total development will access / egress from this point;

Daily trips have assumed to be 50% incoming and 50% outgoing.

Table 4: Number of Trips per Access Point

Access Point	Daily Trips IN	Daily Trips OUT	AM Peak Trips IN	AM Peak Trips OUT	PM Peak Trips IN	PM Peak Trips OUT
AP1	200	200	4	36	36	4
AP2	67	67	2	12	12	2
Total	267	267	6	48	48	6

The generated traffic at each AP has is visualised below in Figure 15 (AM Peak) and Figure 16 (PM Peak) based on the above assumptions. The generated traffic distribution onto Mooringe Avenue via Streeters Road is shown in Figure 17 (AM Peak) and Figure 18 (PM Peak).

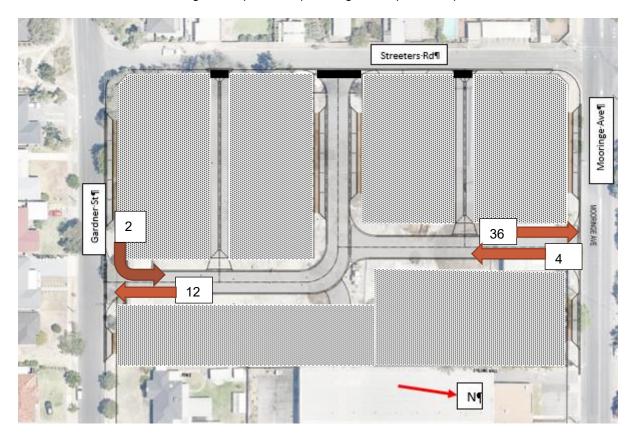


Figure 15: Internal Traffic Generation – AM / Morning Peak Hour

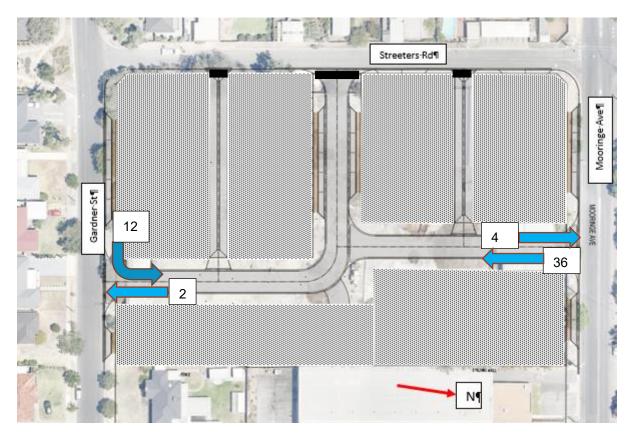


Figure 16: Internal Traffic Generation – PM / Afternoon Peak Hour

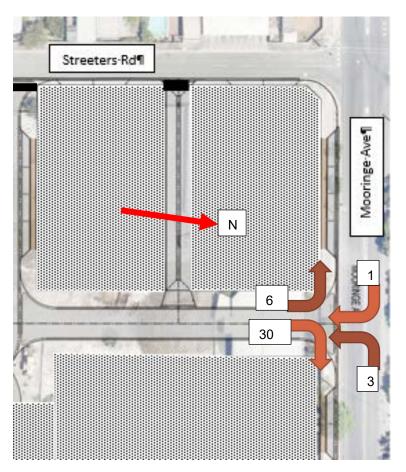


Figure 17: Development Traffic onto Mooringe Ave AM Peak

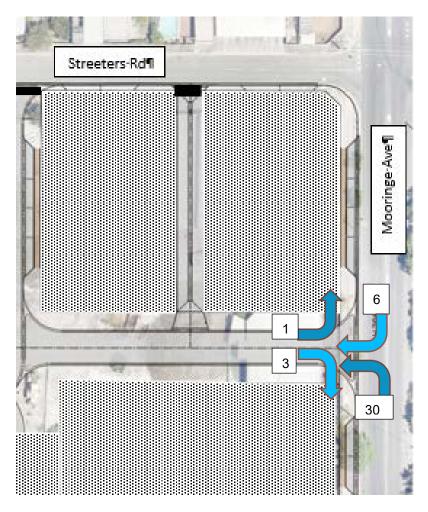


Figure 18: Development Traffic onto Mooringe Ave PM Peak

Table 5 and 6 demonstrate the new demand at the intersection of Streeters Road and Mooringe Avenue following the proposed completion of the Rezoning. The volumes are based upon the turning count undertaken on 3 April 2018, with the AM peak volumes assuming a reversal of volumes IE eastbound traffic on Mooringe Avenue in the PM peak converts to westbound traffic in the AM peak. Right turn out of Streeters Avenue (westbound) in the PM peak converts to left turn in (northbound) etc. The volumes have had the Rezoning trips added to their respective movement (represented within the brackets).

The Sidra Modelling also applies some sensitivity testing by increasing all entering volumes by 5% for all movements on all legs, both for existing and post development analysis.

Table 5: Mooringe Ave / Streeter	s Road AM Peak Hour proposed	I distribution post development
Table 6. Mooninge / We / Bliceler	o noud mini i can nour proposed	alouibation pool acvelopment

Road	Leg	Intersection Behaviour			
Roud	209	Straight	Left	Right	
Mooringe Avenue	West	495	83	(0+1) = 1	
Mooringe Avenue	East	334	(0+1) = 1	30	
Streeters Road	South	2	(0+2) = 2	(0+10) = 10	
Streeters Road	North	0	25	40	

Table 6: Mooringe Ave / Streeters Road PM Peak Hour proposed distribution post development

Road	Leg	Intersection Behaviour			
Koau	209	Straight	Left	Right	
Mooringe Avenue	West	334	40	(0+2) = 2	
Mooringe Avenue	East	495	(0+10) =10	25	
Streeters Road	South	0	(0+1) = 1	(0+1) = 1	
Streeters Road	North	2	30	83	

Table 7: Access Point 1 AM Peak Hour proposed distribution post development

Road	Leg	Intersection Behaviour			
Nodu	209	Straight	Left	Right	
Mooringe Avenue	West	495	NA	(1+1) =2	
Mooringe Avenue	East	334+30=374	(0+3) = 3	NA	
Access Point 1	South	NA	6	30	

Table 8: Access Point 1 PM Peak Hour proposed distribution post development

Road	Leg	Intersection Behaviour			
Nodu	209	Straight	Left	Right	
Mooringe Avenue	West	334	NA	(0+6) = 6	
Mooringe Avenue	East	495+25=520	(0+30) =30	NA	
Access Point 1	South	NA	1	3	

The impact of the Rezoning's generated traffic on the Mooringe Avenue / Marion Road intersection was also considered, as shown in figure 19 below.

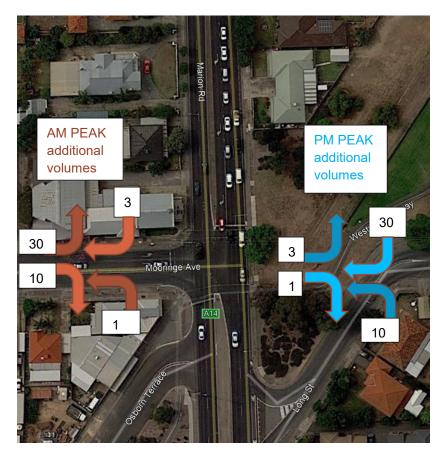


Figure 19 – Additional Trip Generation on Marion Road – AM and PM peak

Table 9: Marion Road / Mooringe Road Signals AM Peak Hour proposed distribution post development

Road	Leg	Intersection Behaviour		
		Straight	Left	Right
Mooringe Avenue	West	NA	(427+30) = 457	(223+10) = 233
Marion Road	North	854	NA	(260+3) = 263
Marion Road	South	1476	(99+1) = 100	NA

 Table 10: Marion Road / Mooringe Road Signals PM Peak Hour proposed distribution post

 development

Road	Leg	Intersection Behaviour		
		Straight	Left	Right
Mooringe Avenue	West	NA	(206+3) = 209	(210+1) = 211
Marion Road	North	1151	NA	(257+30) = 287
Marion Road	South	992	(147+10) = 157	NA

O DEVELOPMENT ACCESS ARRANGEMENTS

The Rezoning assessment has assumed that the three proposed access points as discussed in Section 4. These accesses will be assessed against Austroads Guide to Traffic Management Part 6 – Intersections, Interchanges and Crossings (AGTM06-17) Figure 2.26(c) and Austroads Guide to Road Design Part 4A – Unsignalised and Signalised Intersections (AGRD04A-17) to finalise the junction layouts. The existing AADT volumes can be found in Section 3.1 and generated traffic in Section 5.3.

Access Point 1 (AP1) is proposed on Mooringe Road, and caters for the highest turning volumes, therefore it is considered to be the "critical" access.

Figure 20 below suggests that with a maximum of 30 vehicles/hour turning left into the Rezoning at AP1 (exceeding the volumes for any other access point and equalling the proposed volumes at Mooringe Avenue intersection with Streeters Road), the warrant for turning facilities has been triggered for an AUL(S) for the left in movement. The dimensions for an AUL(S) for the relevant 60km/h speed zone (Mooringe Avenue), are indicated in Figure 20.

In this instance Mooringe Avenue westbound lane is already a total of 6.0m in width. The existing roadway width provides sufficient space to pass a left turning vehicle without delaying the through lane traffic, provided that this road width is maintained on Mooringe Avenue for 35m on westbound approach to AP1 (note the proposed rezoning indicates indented parking on Mooringe Avenue adjacent to the development). The offset between Streeters Road and AP1 is 55m.

Austroads Guide to Road Design Part 4 *Intersections and Crossings* discusses the minimum spacing of driveways in Appendix E Table E3. For a design speed of 60km/h the minimum spacing is 30m and desirable spacing is 40m between access points (AP1 and Streeters Road), therefore the spacing between AP1 and Streeters Road exceeds the requirement. Even when a design speed of 70km/h is adopted, 55m is indicated to be the desirable spacing.

The 55m also provides sufficient distance for a through vehicle on Mooringe Avenue heading westbound to weave between a slowing left turning vehicle into AP1, then shift laterally to the left to avoid vehicles (up to 5 queuing vehicles) right turning into Streeters Road (heading northbound). According to the Taper Equation only 20m is required (refer to Figure 21). In addition, it would be considered unreasonable to impose an Auxiliary Left Turn Treatment on this proposal at AP1, when many side roads along Mooringe Avenue have much higher levels of "left in" turning volumes.

Figure 20 below also suggests that with a maximum of 12 vehicles/hour turning left into the Rezoning at AP2, the warrant for turning facilities is not met to require a painted turn lane, until the AADT on Streeter's Road or Gardner Street exceed approximately 6000 VPD, which is not likely to occur for the foreseeable future.

The highest volume for right in turns is a maximum of 6 vehicles/hour for AP1, this is within the Basic Auxiliary Right (BAR) level.

Basic Auxiliary Right (BAR) / Basic Auxiliary Left (BAL) treatments cannot be conveniently provided where the road is kerbed, and existing driveways are located opposite to the new access. However, Council could consider some parking bans to ensure area is free of standing vehicles around the proposed access points to undertake manoeuvring around turning vehicles.

Therefore, no junction treatments are required at proposed AP1, AP2. Some minor linemarking revisions on Mooringe Avenue could be undertaken to differentiate Access Point 1.

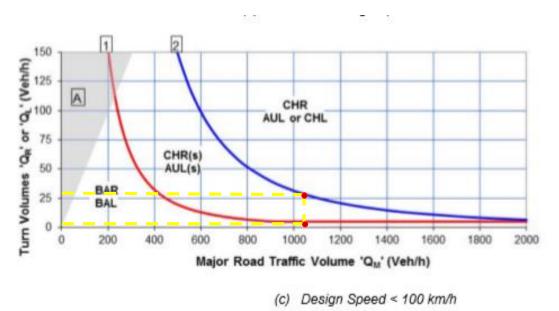


Figure 20: Major Road Turn Treatments Design Speed (suitable for urban environments)

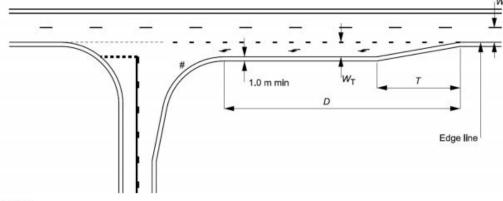


Figure 8.3: Rural AUL(S) treatment with a short left-turn lane

Notes:

- # For setting out details of the left-turn geometry, use vehicle turning path templates and/or Table 8.2.
- Approaches to left-turn slip lanes can create hazardous situations between cyclists and left-turning motor vehicles.
- Treatments to reduce the number of potential conflicts at left-turn slip lanes are given in AGRD Part 4 (Austroads 2017). The dimensions of the treatment are defined as follows. Values of D and T are provided in Table 8.2.
 - W = Nominal through lane width (m) (including widening for curves). For a new intersection on an existing road, the width is to be in accordance with the current link strategy.
 - W_T = Nominal width of the turn lane (m), including widening for curves based on the design turning vehicle = 3.0 m minimum.
 - T = Physical taper length (m) given by Equation 5 being: $T = \frac{0.33VW_{T}}{3.6}$
 - V = Design speed of major road approach (km/h).

Source: Department of Main Roads (2006)37.

Design speed of major road approach (km/h)	Diverge/deceleration length D (m) ¹	Taper length 7 (m) ²
50	15	15
60	25	15
70	35	20
80	45	20
90	55	25
100	70	30
110	85	30
120	100	35

Table 8.2: Dimensions for AUL(S) treatment on major leg

1 Based on a 20% reduction in through road speed at the start of the taper and a value of deceleration of 3.5 m/s² (Table 5.2). Adjust for grade using the 'correction to grade', (Table 5.3).

2 Based on a turn lane width of 3.0 m.

Source: Department of Main Roads (2006)38.

Figure 21: Dimensions for an AUL(S)

W = 6.0m (width available kerb to centreline at this location)

W⊤ = 3.0m

T = (0.33 X 70 X 3.0) / 3.6 = 19.25m (say 20m)

D = 35m

ACCESS ANALYSIS

7.1 MOORINGE AVENUE INTERSECTION STREETERS ROAD ANALYSIS

SIDRA Intersection 7.0 was utilised for the assessment the existing intersections influenced by the proposed Rezoning, for morning and afternoon peak hour periods.

Figures 21 shows the simple intersection layout that the model is based on.

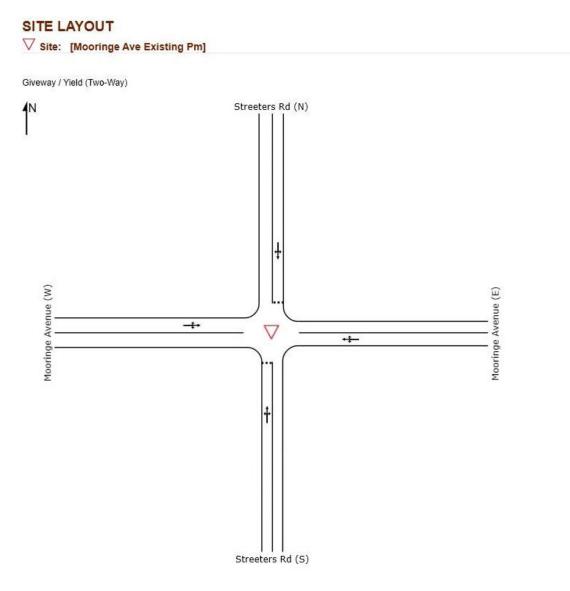


Figure 21: Diagrammatic representation of the Sidra Intersection model

Table 9 and 10 below present a summary of the pre and post development operation of the unsignalised Mooringe Avenue / Streeters Road Intersection for the morning and afternoon periods respectively.

Lane	Degree of Saturation	Average Delay (sec)	Queue Distance (m)	Level of Service
Streeters Rd (S) Existing	0.01	10.7	0.2	В
Streeters Rd (S) Post Development	0.038	12.4	0.8	В
Mooringe Ave (E) Existing	0.210	1.3	3.4	NA
Mooringe Ave (E) Post Development	0.214	1.3	3.2	NA
Streeters Rd (N) Existing	0.158	12.3	3.7	В
Streeters Rd (N) Post Development	0.158	12.3	3.7	В
Mooringe Av (W) Existing	0.303	0.8	0.1	NA
Mooringe Av (W) Post Development	0.303	0.8	0.1	NA
Intersection Existing	0.303	1.8	3.7	NA
Intersection Post Development	0.303	1.9	3.7	NA

Table 9: Summary: Morning Peak Hour (Shaded Post Development)

Table 10: Summary: Afternoon Peak Hour (Shaded Post Development)

Lane	Degree of Saturation	Average Delay (sec)	Queue Distance (m)	Level of Service	
Streeters Rd (S) Existing	0.006	10.4	0.1	В	
Streeters Rd (S) Post Development	0.007	10.5	0.3	В	
Mooringe Ave (E) Existing	0.287	0.6	2.3	NA	
Mooringe Ave (E) Post Development	0.292	0.6	2.4	NA	
Streeters Rd (N) Existing	0.287	13.7	7.8	В	
Streeters Rd (N) Post Development	0.286	13.6	7.7	В	
Mooringe Av (W) Existing	0.199	0.7	0.1	NA	
Mooringe Av (W) Post Development	0.199	0.7	0.3	NA	
Intersection Existing	0.287	2.1	7.8	NA	
Intersection Post Development	0.292	2.1	7.7	NA	

The SIDRA analysis shows that the current average delay for the Streeters Road North Leg was around 12-14 seconds. This is commensurate with the observations on site.

The results shown in the above tables indicate the intersection would operate satisfactorily if the proposed Rezoning were to go ahead, and that the intersection adequately facilitates the relatively free flow of traffic during morning and afternoon peak periods, with only minimal queues forming in Streeters Road (south) post development, and very little change in flows for Streeters Road (north) – however the difference in intersection performance would be virtually imperceptible to road users.

In conclusion, the SIDRA analysis shows that even using a highly conservative model with all development traffic filtered through the one intersection and 5% growth applied, the performance of the unmodified local network will adequately cope with the proposed development trip generation.

7.2 MOORINGE AVENUE INTERSECTION ACCESS POINT 1 ANALYSIS

SIDRA Intersection 7.0 was utilised for the assessment the proposed access point onto Mooringe Avenue for the proposed Rezoning, for morning and afternoon peak hour periods.

Figure 22 below shows the simple junction layout that the model is based on.

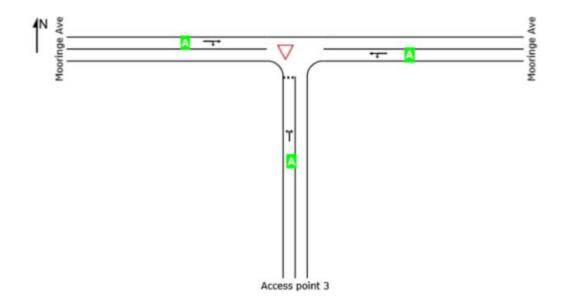


Figure 22: Diagrammatic representation of the Sidra Intersection model

Access Point 1 (AP1) was modelled for its impact on Mooringe Avenue. Table 11 & 12 show the results from SIDRA Intersection 7.0 analysis of this proposed access point.

Lane	Degree of Saturation	Average Delay (sec)	Queue Distance (m)	Level of Service
Access Point 1	0.056	7.7	1.3	A
Mooringe Ave (E) Post Development	0.217	5.6	0	NA
Mooringe Ave (W) Post Development	0.272	0	0.2	NA
Intersection Post Development	0.272	2.6	1.3	NA

Table 11: Summary: Morning Peak Hour

Lane	Degree of Saturation	Average Delay (sec)	Queue Distance (m)	Level of Service
Access Point 1	0.005	6.8	0.1	A
Mooringe Ave (E) Post Development	0.315	5.6	0.0	NA
Mooringe Ave (W) Post Development	0.189	0.2	0.6	NA
Intersection Post Development	0.315	3.4	0.6	NA

The results of the analysis indicate that the proposed Access Point 1 onto Mooringe Avenue will operate with minimal delays to the new access point and present no expected traffic issues for Mooringe Avenue.

7.3 MOORINGIE AVENUE INTERSECTION MARION ROAD

SIDRA Intersection 7.0 was utilised for the assessment of the effects of proposed generated additional traffic from the proposed Rezoning at the Mooringe Avenue intersection with Marion Road, for morning and afternoon peak hour periods.

Figures 23 below shows the signalised junction layout that the model is based on.

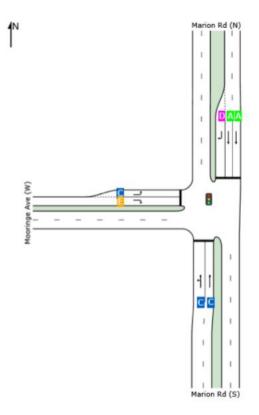


Figure 23: Diagrammatic representation of the Sidra Intersection model (Existing AM Peak LOS shown)

Table13 and 14 below present a summary of the pre and post development operation of the Mooringe Avenue / Marion Road Signalised Intersection for the morning and afternoon periods respectively.

Lane	Degree of Saturation	Average Delay (sec)	Queue Distance (m)	Level of Service
Marion Rd (S) Existing	0.839	29.7	315.8	С
Marion Rd (S) Post Development	0.853	32.2	329.5	С
Marion Rd (N) Existing	0.328	16.4	64.4	В
Marion Rd (N) Post Development	0.691	17.1	108.8	В
Mooringe Av (W) Existing	0.832	52.3	179.6	D
Mooringe Av (W) Post Development	0.869	54.8	204.9	D
Intersection Existing	0.839	29.7	315.8	С
Intersection Post Development	0.869	31.8	329.5	С

Table 13: Summary: Morning Peak Hour (Shaded Post Development)

 Table 14: Summary: Afternoon Peak Hour (Shaded Post Development)

Lane	Degree of Saturation	Average Delay (sec)	Queue Distance (m)	Level of Service
Marion Rd (S) Existing	0.699	29.0	210.0	С
Marion Rd (S) Post Development	0.719	30.0	215.8	С
Marion Rd (N) Existing	0.444	13.0	100.7	В
Marion Rd (N) Post Development	0.557	13.4	104.6	В
Mooringe Av (W) Existing	0.289	42.8	90.6	D
Mooringe Av (W) Post Development	0.737	43.6	93.9	D
Intersection Existing	0.699	23.3	210.0	С
Intersection Post Development	0.737	23.9	215.8	С

The results of the analysis show that the performance of the Marion Road signalised intersection with Mooringe Avenue is only marginally affected by the increased volumes from the proposed rezoning. The greatest affects of the rezoning are shown in the AM peak, with queues on Mooringe Avenue expected to increase by 25m and Marion Road North leg by 40m. The probability of queues exceeding the allocated short left turn lane storage on Marion Road (South leg) increase from existing 50% to proposed 55% in the AM peak and from 13% to 16% in the PM Peak. However, the level of service remains the same for either leg and incurred additional delays are expected to be minimal.

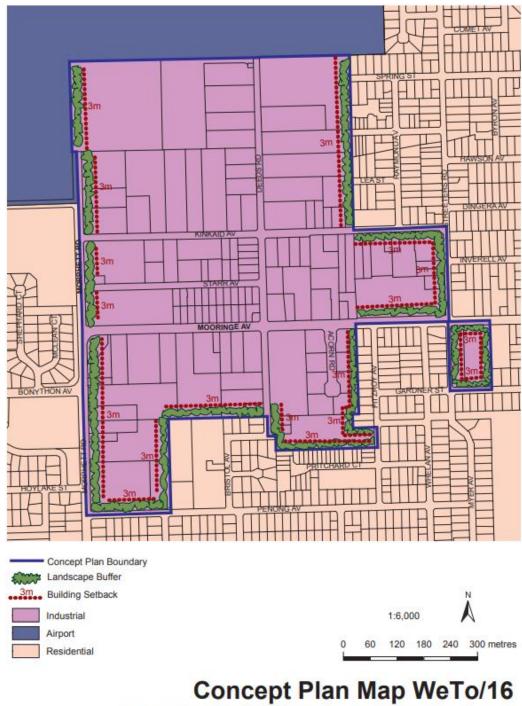
SUMMARY AND CONCLUSIONS

The traffic assessment has provided a background on the existing conditions of the site, the likely traffic generated by the proposed rezoning and its impacts on the external road network. From the assessment, the following key findings and recommendations are summarised below:

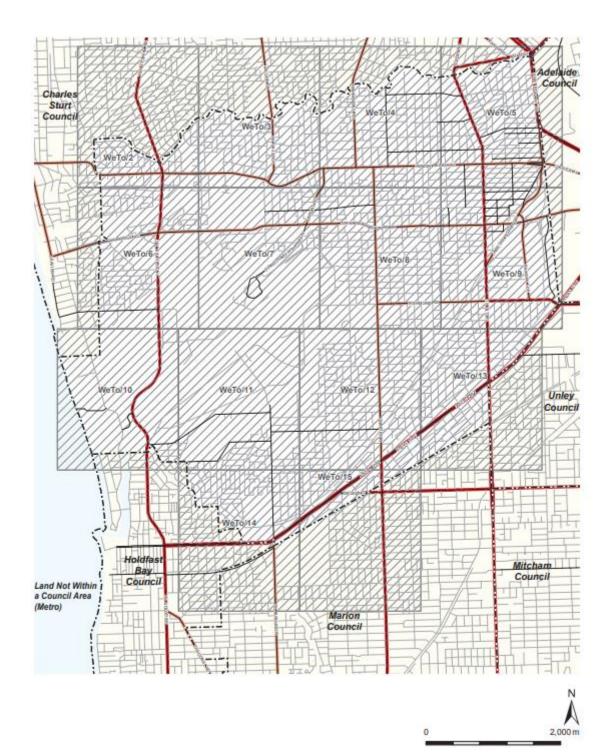
- The proposed rezoning is proposed to amend land use from industrial to residential in the form of medium density townhouses. The Rezoning proposes an internal road access of approximately 2300 square meters of road network, accessing via two access points (Gardner Street and Mooringe Avenue). The Rezoning's internal road network still requires detail design and assessment.
- The proposed rezoning would likely increase local area traffic by around 533 vehicles per day, with around 54 vehicle trips generated during peak hour traffic.
- The majority of the Rezoning traffic will access the arterial road network directly from Access Point 1 (AP1 via Mooringe Avenue), however it is likely that some development traffic will redistribute to Whelan Avenue and Errington Street via Access Point 2 (Gardner Road), potentially lessening the volumes placed on AP1 assumed in the traffic model.
- The Rezoning has no impact on programmed road upgrades in the area, nor do any programmed upgrades impact the proposal. Given the narrow verge on Streeters Road, Council's proposal to widen Streeters Road will likely benefit traffic behaviour for the Rezoning but requires further assessment to gauge the impact on the proposal. Council has suggested that land could be provided from the subject site to enable a wider verge to be provided to accommodate future footpath and landscaping requirements.
- The existing road network flows reasonably well during peak hour, with observations indicating only minor increase in delays experienced for traffic entering Mooringe Avenue from adjacent side roads.
- Crash history indicates that crashes in the vicinity of the Rezoning are at established "conflict points" IE intersections and junctions. All intersections and junctions reviewed are considered to be performing adequately for the types of intersection and volumes experienced.
- The Rezoning site is already well serviced by existing public transport modes and reasonably good connections to cycling and pedestrian facilities and networks within the local area. Internal road network design should consider the requirements in the CWTDP for pedestrian and cyclist connectivity to infrastructure.
- The City of West Torrens has determined that the rezoning will fit under Residential Medium Density Policy Area 18, and the parking requirement would be determined by PDC12 and 16, and Table WeT0/2. In essence this requires 1 covered and 1 uncovered off-street park and 0.5 on-street parks, per dwelling.

- All sight distances are likely to be achieved for the proposed access points onto Mooringe Avenue, Streeters Road and Gardner Avenue.
- In consideration of the Austroad Guidelines, the proposed Access Points for the Rezoning do not warrant and will not require any turning treatments for Mooringe Avenue, Streeters Road or Gardner Street. The 55m separation between Access Point 1 and Streeters Road meets Austroads Guidelines.
- Traffic modelling (SIDRA) indicates that the Mooringe Avenue / Streeters Road Intersection
 performs to an acceptable level of service for the estimated post-development traffic flows. Traffic
 performance will remain similar to existing levels of service, creating only minimal delays to traffic
 on the minor legs of the intersection. No significant changes to the Mooringe Avenue / Streeters
 Road Intersection are required to cater for the traffic impacts generated by the Rezoning.
- Traffic modelling (SIDRA) indicates that the Mooringe Avenue / Access Point 1 Intersection
 performs to a good level of service for the estimated post-development traffic flows. Traffic flow on
 Mooringe Avenue will be generally unimpeded and delays to the traffic queuing out of Access Point
 1 are expected to be minimal. No significant changes to the proposed Mooringe Avenue / Access
 Point 1 Intersection are required to cater for the traffic impacts generated by the Rezoning.
- Traffic modelling for the Mooringe Avenue / Marion Road Traffic Signals with the anticipated 54 veh/hr increase during peak times, indicated minimal impact on the performance of the signalised intersection with levels of service remaining the same.

APPENDIX A CWTDP REFERENCES



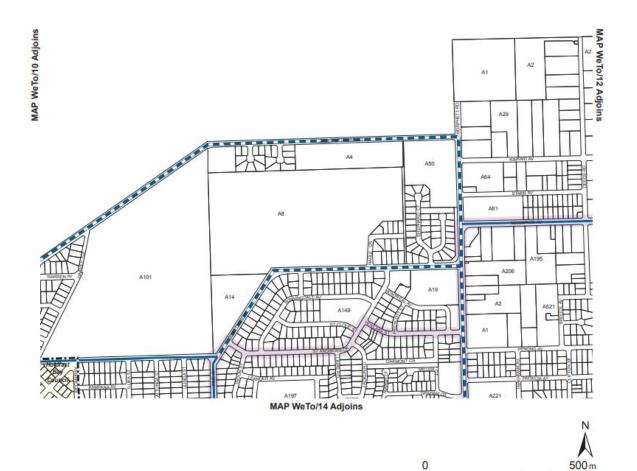
NORTH PLYMPTON / CAMDEN PARK INDUSTRY



Overlay Map WeTo/1 TRANSPORT

Primary Arterial Roads Secondary Arterial Roads Development Plan Boundary

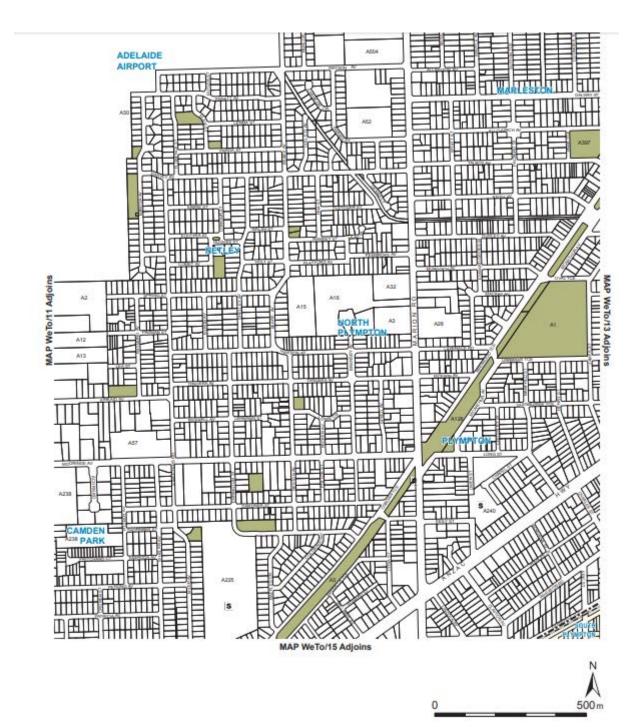
Consolidated - 12 July 2018



Overlay Map WeTo/11 TRANSPORT

WEST TORRENS COUNCIL Consolidated - 12 July 2018

Bikedirect Network Secondary Road - Bike Lane Secondary Road Public Transport Development Plan Boundary



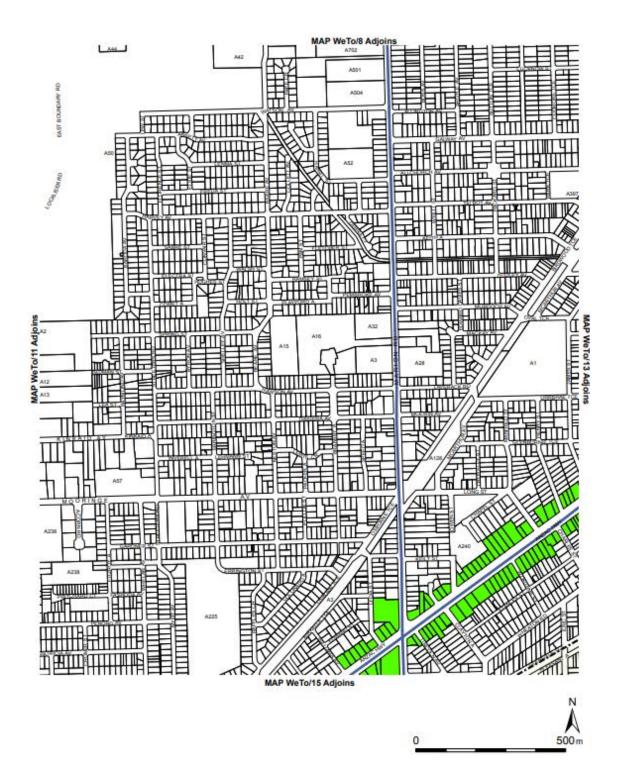
Location Map WeTo/12

School
 Post Office
 Railways
 Local Reserves
 Development Plan Boundary



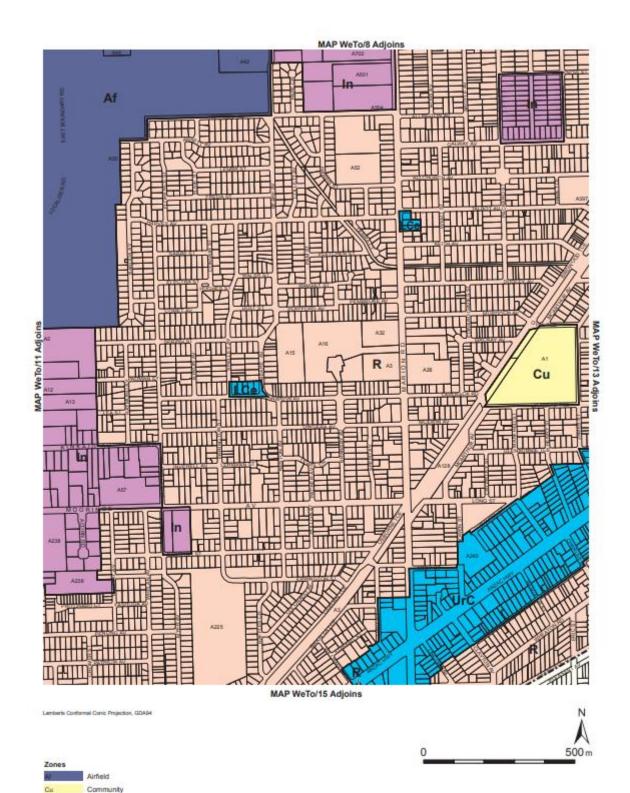
Primary Arterial Roads Secondary Arterial Roads Bikedirect Network Main Road - Bike Lane Main Road Secondary Road - Bike Lane Secondary Road Off Road Sealed Path Public Transport Development Plan Boundary

Overlay Map WeTo/12 TRANSPORT



Overlay Map WeTo/12 STRATEGIC TRANSPORT ROUTES

Strategic Transport Route Strategic Transport Routes Designated Area

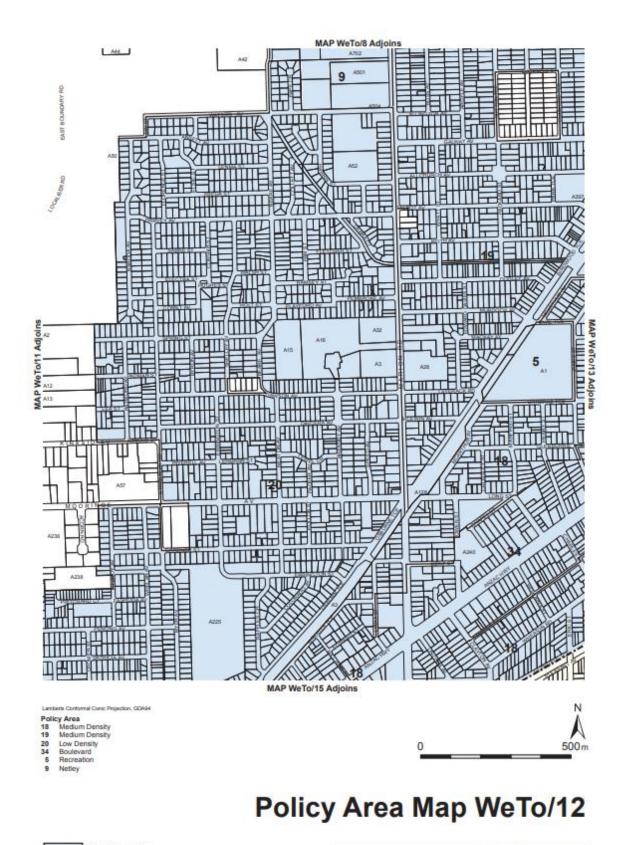


industry

Local Centre Residential Urban Corridor Zone Boundary

Development Plan Boundary

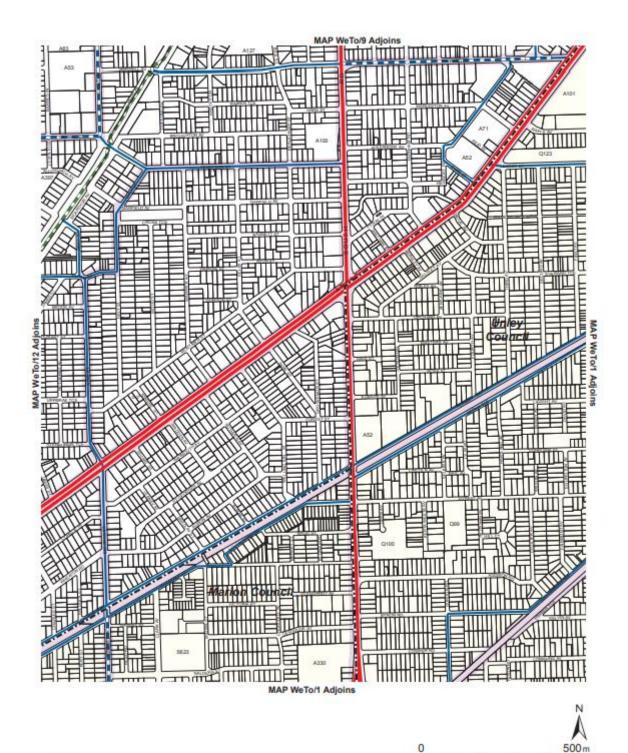
Zone Map WeTo/12



WEST TORRENS COUNCIL Consolidated - 12 July 2018

Policy Area Boundary

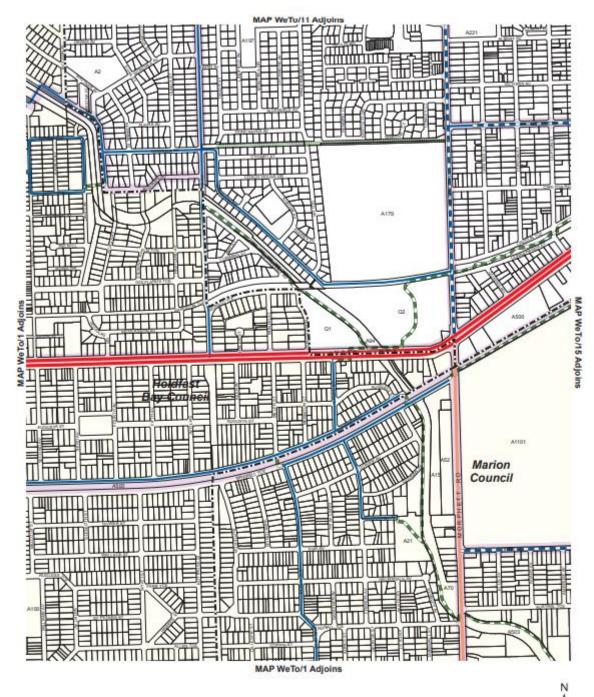
Development Plan Boundary



Overlay Map WeTo/13 TRANSPORT

WEST TORRENS COUNCIL Consolidated - 12 July 2018

Primary Arterial Roads Bikedirect Network Main Road - Bike Lane Main Road Secondary Road - Bike Lane Secondary Road Off Road Sealed Path Public Transport Development Plan Boundary



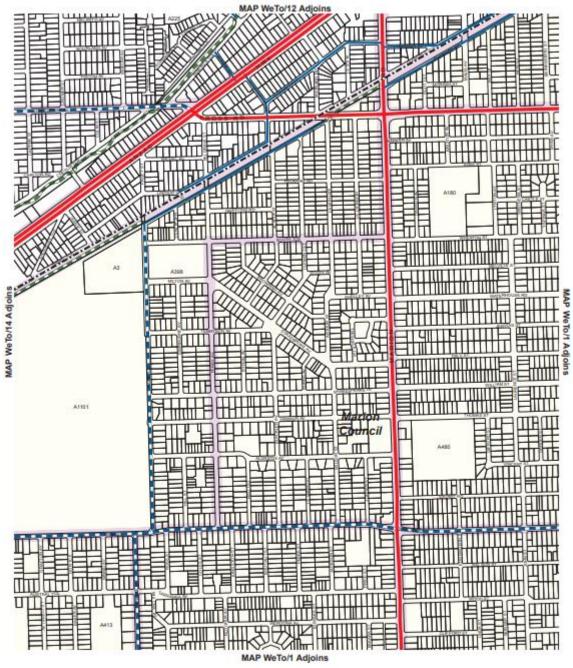
	A
0	500 m

Overlay Map WeTo/14 TRANSPORT

WEST TORRENS COUNCIL Consolidated - 12 July 2018

_	Primary Arterial Roads
-	Secondary Arterial Roads
Bikedirect N	etwork
	Main Road - Bike Lane
	Main Road
	Secondary Road - Bike Lane
	Secondary Road
	Off Road Sealed Path
	Off Road Track
	Public Transport
	Development Dive Development

----- Development Plan Boundary





Overlay Map WeTo/15 TRANSPORT

WEST TORRENS COUNCIL Consolidated - 12 July 2018

Primary Arterial Roads Bikedirect Network Main Road - Bike Lane Main Road - Bike Lane Secondary Road - Bike Lane Secondary Road - Bike Lane Off Road Sealed Path Off Road Track Public Transport Development Plan Boundary

APPENDIX B DPTI VEHICLE TURNING MOVEMENT SURVEY (2011&2017)

	CHELMO /0670 - v10	05 Department of Planning, Transport a Vehicle Turning Movement											Page 1 of 1 23/05/2017 10:18			
L AMG Ref Date of	tion of: MA ocality: PL erence: TG Count: 17/ /eather: Dry Status:	YMPTO 766285 05/2017	N	Day:	GE AVEN Wednes SIGNAL	sday								Arm 1 2 3	Road Number - Name 6601 - MARION ROAD 6601 - MARION ROAD 6598 - MOORINGE AVENUE	
	Arm	1		2		3]							I C	
	Exit Arm	2	3 (R)	3 (L)	1	1 (L)	2 (R)								MOORINGE AV	
11 hour	Cars	9527	2130	1249	10568	2241	1725								3 5	
totals	CV	463	285	115	506	266	134	-							3	
	Total	9990	2415	1364	11074	2507	1859								MARION RN6601	
AM Peak hour		811	236	93	1429	399	207								RN6601 C	
(08:15)	CV	43	24	6	47	28	16	-							2	
	Total	854	260	99	1476	427	223									
PM Peak hour		1127	230	130	942	185	203	-							7 11	
(15:15)	CV	24	27	17	50	21	7	-								
	Total	1151	257	147	992	206	210									
					1				2				3			
One-	11 Hc	our Total	s (IN) 12405	(OUT)	13581	(IN) 12	438	(OUT)	11849	(IN) 43	866	(OUT)	3779	_	
way Flows	AM P	eak Hou	ır 08 :	00 111	8 08:15	1903	06:45	1580	08:00	1087	08:00	677	08:15	359	_	
	PM P	eak Hou	ır 16 :	30 155	5 15:15	1198	15:15	1139	16:30	1412	14:45	452	17:00	434	_	
Two-	AM P	eak Hou	ır	08:15	301	7	0	8:15	265	2	08	8:00	102	2		
way Flows	PM P	eak Hou	ır	15:15	260	6	1	5:15	250	0	1	4:45	879			
All	11 Hc	our Total	s	25986	5.8%	CV	242	287	5.0%	CV	814	5	9.8% (V		
Vehicles	Estima	ated AAE	DT 33	500 SF(1.00) ZF	(1.29)	31300	SF(1	.00) ZF(1.29)	10500	SF(1	.00) ZF(1.29)	-	

AADT - Annual Average Daily Traffic SF - Seasonal Factor ZF - Zone Factor CV - Commercial Vehicles

T∨ TV	′S ⁄0670		TRANSPORT SA Vehicle Turning Movement Survey													Page 1 of 1 05/10/2000 11:35	
Intersec I Date o W	ction of: tion No: _ocality: f Count: /eather: nditions:	MARIO TG7662 PLYMP 21/08/1 Dry SIGNAI	285 TON 997	MOORIN Day:	GIE AVE Thursda							Arm 1 2 3	6 6	Road Number - Name 6601 - MARION RD 6601 - MARION RD Mooringie Ave		6601	
	Arm	1		2		3		1								1	
	Exit Ar	2	3 (R)	3 (L)	1	1 (L)	2 (R)										
11 hour	Cars	8920	2094	971	9084	2379	1341								Mooringe Ave		
totals C	CV	513	319	89	452	324	94								3		
	Total	9433	2413	1060	9536	2703	1435									2	
AM Peak		619	154	75	1493	447	162]								o	
hour (07:45)	CV	54	20	8	48	31	9	_							al al	6601	
	Total	673	174	83	1541	478	171								1	01	
PM Peak hour		1301	406	69	665	174	134	_									
(16:45)	CV	30	20	1	22	15	2	-									
	Total	1331	426	70	687	189	136										
					1				2			3					
One-way Flows	11 H	lour Total	s (IN) 11846	(OUT) 12239	(IN) 10	596	(OUT) 10868	(IN) 41	38	(OUT) 3473	3				
	AM F	Peak Hou	ır 11	:00 970	07:30	2091	07:30	1716	11:00 883	07:45	649	11:00 324	4				
	PM F	Peak Hou	ır 16	:45 175	57 15:00	0 990	14:00	849	16:45 1467	15:00	472	17:00 506	6				
Two-way	AM I	Peak Hou	ır	07:45	28	66	0	7:45	2468	07	7:45	906					
Flows	PM I	Peak Hou	ır	16:45	26	33	1	6:45	2224	15	5:00	847					
All	11 H	lour Total	s	24085	6.7%	CV	214	464	5.3% CV	7611	1	10.9% CV					

All Vehicles Estimated AADT 9650 SF(1.00) ZF(1.27) 30600 SF(1.00) ZF(1.27) 27300 SF(1.00) ZF(1.27)

AADT - Average Annual Daily Traffic SF - Seasonal Factor

ZF - Zone Factor

APPENDIX C SIDRA RESULTS

INTERSECTION SUMMARY

 ∇ Site: [Mooringe Ave post Am]

Giveway / Yield (Two-Way)

Intersection Performance - Hourly Values		
Performance Measure	Vehicles	Persons
Travel Speed (Average)	57.9 km/h	57.9 km/h
Travel Distance (Total)	1089.8 veh-km/h	1307.8 pers-km/h
Travel Time (Total)	18.8 veh-h/h	22.6 pers-h/h
Demand Flows (Total)	1078 veh/h	1293 pers/h
Percent Heavy Vehicles (Demand)	2.0 %	1295 pers/ii
Degree of Saturation	0.303	
Practical Spare Capacity	222.9 %	
Effective Intersection Capacity	3552 veh/h	
Control Delay (Total)	0.56 veh-h/h	0.67 pers-h/h
Control Delay (Average)	1.9 sec	1.9 sec
Control Delay (Worst Lane)	12.4 sec 15.1 sec	15.1 sec
Control Delay (Worst Movement) Geometric Delay (Average)	1.1 sec	15.1 Sec
Stop-Line Delay (Average)	0.8 sec	
Idling Time (Average)	0.4 sec	
Intersection Level of Service (LOS)	NA	
95% Back of Queue - Vehicles (Worst Lane)	0.5 veh	
95% Back of Queue - Distance (Worst Lane)	3.7 m	
Queue Storage Ratio (Worst Lane)	0.00	470
Total Effective Stops Effective Stop Rate	144 veh/h 0.13 per veh	172 pers/h 0.13 per pers
Proportion Queued	0.13 per ven 0.11	0.13 per pers 0.11
Performance Index	21.7	21.7
Cost (Total)	428.91 \$/h	428.91 \$/h
Fuel Consumption (Total)	74.2 L/h	
Carbon Dioxide (Total)	175.5 kg/h	
Hydrocarbons (Total) Carbon Monoxide (Total)	0.013 kg/h 0.214 kg/h	
NOx (Total)	0.214 kg/h	
	0.100 Ng/11	

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). NA: Intersection LOS for Vehicles is Not Applicable for two-way sign control since the average intersection delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Intersection Performance - Annual Va	alues	
Performance Measure	Vehicles	Persons
Demand Flows (Total)	517,390 veh/y	620,867 pers/y
Delay	269 veh-h/y	323 pers-h/y
Effective Stops	68,973 veh/y	82,768 pers/y
Travel Distance	523,127 veh-km/y	627,752 pers-km/y
Travel Time	9,043 veh-h/y	10,851 pers-h/y
Cost	205,878 \$/y	205,878 \$/y
Fuel Consumption	35,625 L/y	-
Carbon Dioxide	84,250 kg/y	
Hydrocarbons	6 kg/y	
Carbon Monoxide	103 kg/y	
NOx	78 kg/y	

MOVEMENT SUMMARY

✓ Site: [Mooringe Ave post Am]

Giveway / Yield (Two-Way)

Move	ement Pe	erformance	- Vehic	les							
Mov ID	OD Mov	Demand I Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h
South	: Streeter	s Rd (S)									
1	L2	2	0.0	0.038	6.7	LOS A	0.1	0.8	0.65	0.82	48.7
2	T1	2	0.0	0.038	11.7	LOS B	0.1	0.8	0.65	0.82	48.9
3	R2	11	2.0	0.038	13.7	LOS B	0.1	0.8	0.65	0.82	48.2
Appro	ach	15	1.4	0.038	12.4	LOS B	0.1	0.8	0.65	0.82	48.3
East:	Mooringe	Avenue (E)									
4	L2	1	0.0	0.214	9.0	LOS A	0.5	3.2	0.15	0.06	57.2
5	T1	352	2.0	0.214	0.6	LOS A	0.5	3.2	0.15	0.06	58.8
6	R2	32	2.0	0.214	9.0	LOS A	0.5	3.2	0.15	0.06	56.5
Appro	ach	384	2.0	0.214	1.3	NA	0.5	3.2	0.15	0.06	58.6
North	Streeters	s Rd (N)									
7	L2	26	2.0	0.158	7.8	LOS A	0.5	3.7	0.65	0.83	48.7
8	T1	1	0.0	0.158	11.5	LOS B	0.5	3.7	0.65	0.83	49.0
9	R2	42	2.0	0.158	15.1	LOS C	0.5	3.7	0.65	0.83	48.5
Appro	ach	69	2.0	0.158	12.3	LOS B	0.5	3.7	0.65	0.83	48.6
West:	Mooringe	e Avenue (W)									
10	L2	87	2.0	0.303	5.6	LOS A	0.0	0.1	0.00	0.09	57.5
11	T1	521	2.0	0.303	0.0	LOS A	0.0	0.1	0.00	0.09	59.2
12	R2	1	0.0	0.303	7.3	LOS A	0.0	0.1	0.00	0.09	57.2
Appro	ach	609	2.0	0.303	0.8	NA	0.0	0.1	0.00	0.09	58.9
All Ve	hicles	1078	2.0	0.303	1.9	NA	0.5	3.7	0.11	0.13	57.9

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

LANE SUMMARY

✓ Site: [Mooringe Ave post Am]

Giveway / Yield (Two-Way)

Lane Use a	nd Per	forma	ince										
		nand Iows	Cap.	Deg. Satn	Lane Util.	Average Delay	Level of Service	95% Back of	Queue	Lane Config	Lane Length		Prob. Block.
	Total	HV						Veh	Dist				
0 11 01	veh/h	%	veh/h	v/c	%	sec			m		m	%	%
South: Street	ters Rd (S)											
Lane 1	15	1.4	392	0.038	100	12.4	LOS B	0.1	0.8	Full	500	0.0	0.0
Approach	15	1.4		0.038		12.4	LOS B	0.1	0.8				
East: Moorin	ge Aven	ue (E)											
Lane 1	384	2.0	1796	0.214	100	1.3	LOS A	0.5	3.2	Full	500	0.0	0.0
Approach	384	2.0		0.214		1.3	NA	0.5	3.2				
North: Street	ers Rd (N)											
Lane 1	69	2.0	439	0.158	100	12.3	LOS B	0.5	3.7	Full	500	0.0	0.0
Approach	69	2.0		0.158		12.3	LOS B	0.5	3.7				
West: Moorin	nge Aven	ue (N	/)										
Lane 1	609	2.0	2008	0.303	100	0.8	LOS A	0.0	0.1	Full	500	0.0	0.0
Approach	609	2.0		0.303		0.8	NA	0.0	0.1				
Intersectio n	1078	2.0		0.303		1.9	NA	0.5	3.7				

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Lane LOS values are based on average delay per lane.

Minor Road Approach LOS values are based on average delay for all lanes.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road lanes.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

LANE FLOWS

∇ Site: [Mooringe Ave post Am]

Giveway / Yield (Two-Way)

Approac			s (veh/	h)							
South: Str		. ,									
Mov.	L2	T1	R2	Total	%HV	•	Deg.	Lane		Ov.	
From S						Cap. veh/h	Satn	Util. %	SL Ov. %	Lane	
To Exit:	W	Ν	E			ven/m	v/c	70	70	No.	
Lane 1	2	2	11	15	1.4	392	0.038	100	NA	NA	
Approac	2	2	11	15	1.4		0.038				
h											
East: Moo	oringe Av	venue (l	E)								
Mov.	L2	T1	R2	Total	%HV		Deg.	Lane	Prob.	Ov.	
From E						Cap.	Satn		SL Ov.	Lane	
To Exit:	S	W	Ν			veh/h	v/c	%	%	No.	
Lane 1	1	352	32	384	2.0	1796	0.214	100	NA	NA	
Approac	1	352	32	384	2.0		0.214				
h											
North: Str	eeters F	Rd (N)									
Mov.	L2	T1	R2	Total	%HV		Deg.	Lane		Ov.	
From N						Cap.	Satn		SL Ov.	Lane	
To Exit:	E	S	W			veh/h	v/c	%	%	No.	
Lane 1	26	1	42	69	2.0	439	0.158	100	NA	NA	
Approac	26	1	42	69	2.0		0.158				
h											
West: Mo	oringe A	venue (W)								
Mov.	L2	T1	R2	Total	%HV		Deg.	Lane	Prob.	Ov.	
From W						Cap.	Satn	Util.	SL Ov.	Lane	
To Exit:	Ν	Е	S			veh/h	v/c	%	%	No.	
Lane 1	87	521	1	609	2.0	2008	0.303	100	NA	NA	
Approac	87	521	1	609	2.0		0.303				
h											
	Total	%HV [Deg.Sat	n (v/c)							
Intersec											
	1078	2.0		0.303							
tion											

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.

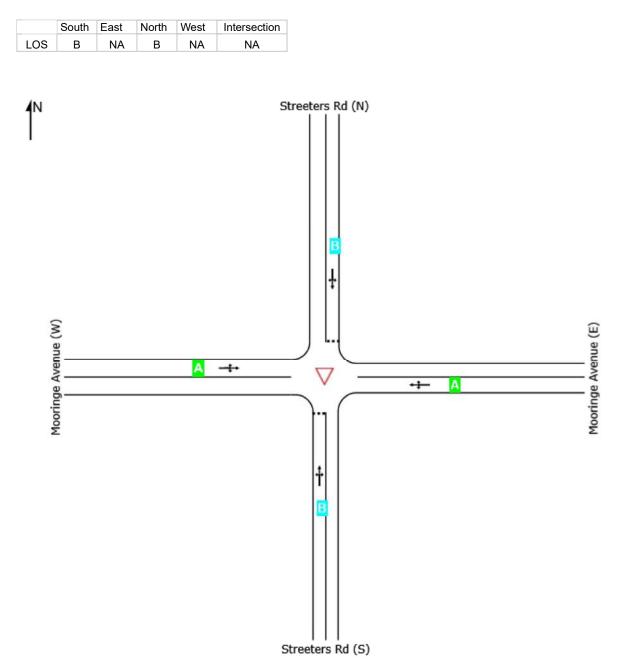
LANE LEVEL OF SERVICE

Lane Level of Service

✓ Site: [Mooringe Ave post Am]

Giveway / Yield (Two-Way)

All Movement Classes



Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Lane LOS values are based on average delay per lane.

Minor Road Approach LOS values are based on average delay for all lanes.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road lanes.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Project: V:\2019\190100 - 190199\190190 - Mooringe Ave\Design\Calculations\Traffic\SIDRA\190190-CA-TT-A-0001[B].sip7

DELAY (CONTROL)

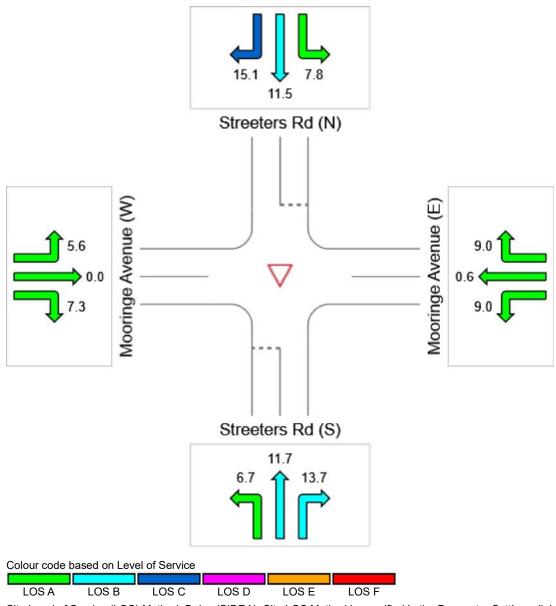
Average control delay per vehicle, or average pedestrian delay (seconds)

✓ Site: [Mooringe Ave post Am]

Giveway / Yield (Two-Way)

All Movement Classes

	South	East	North	West	Intersection
Delay (Control)	12.4	1.3	12.3	0.8	1.9
LOS	В	NA	В	NA	NA



Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

INTERSECTION SUMMARY

✓ Site: [Mooringe Ave & New development AM]

Giveway / Yield (Two-Way)

Intersection Performance - Hourly Values		
Performance Measure	Vehicles	Persons
Travel Speed (Average) Travel Distance (Total) Travel Time (Total)	57.0 km/h 1207.1 veh-km/h 21.2 veh-h/h	57.0 km/h 1448.6 pers-km/h 25.4 pers-h/h
Demand Flows (Total) Percent Heavy Vehicles (Demand) Degree of Saturation Practical Spare Capacity Effective Intersection Capacity	958 veh/h 1.9 % 0.272 259.7 % 3516 veh/h	1149 pers/h
Control Delay (Total) Control Delay (Average) Control Delay (Worst Lane) Control Delay (Worst Movement) Geometric Delay (Average) Stop-Line Delay (Average) Idling Time (Average) Intersection Level of Service (LOS)	0.70 veh-h/h 2.6 sec 7.7 sec 8.4 sec 2.5 sec 0.2 sec 0.1 sec NA	0.84 pers-h/h 2.6 sec 8.4 sec
95% Back of Queue - Vehicles (Worst Lane) 95% Back of Queue - Distance (Worst Lane) Queue Storage Ratio (Worst Lane) Total Effective Stops Effective Stop Rate Proportion Queued Performance Index	0.2 veh 1.3 m 0.00 249 veh/h 0.26 per veh 0.00 22.5	299 pers/h 0.26 per pers 0.00 22.5
Cost (Total) Fuel Consumption (Total) Carbon Dioxide (Total) Hydrocarbons (Total) Carbon Monoxide (Total) NOx (Total)	481.78 \$/h 85.1 L/h 201.2 kg/h 0.015 kg/h 0.240 kg/h 0.189 kg/h	481.78 \$/h

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). NA: Intersection LOS for Vehicles is Not Applicable for two-way sign control since the average intersection delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Performance Measure	Vehicles	Persons
Demand Flows (Total)	459,790 veh/y	551,747 pers/y
Delay	336 veh-h/y	403 pers-h/y
Effective Stops	119,618 veh/y	143,542 pers/y
Travel Distance	579,426 veh-km/y	695,311 pers-km/y
Travel Time	10,169 veh-h/y	12,203 pers-h/y
Cost	231.256 \$/y	231,256 \$/y
Fuel Consumption	40,855 L/y	
Carbon Dioxide	96,592 kg/y	
Hydrocarbons	7 kg/y	
Carbon Monoxide	115 kg/y	
NOx	91 kg/y	

MOVEMENT SUMMARY

V Site: [Mooringe Ave & New development AM]

Giveway / Yield (Two-Way)

Move	ment Pe	rformance	- Vehic	les							
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h
South	: Access p	oint 1									
1	L2	6	0.0	0.056	4.6	LOS A	0.2	1.3	0.03	0.56	44.8
3	R2	32	0.0	0.056	8.4	LOS A	0.2	1.3	0.03	0.56	45.4
Appro	ach	38	0.0	0.056	7.7	LOS A	0.2	1.3	0.03	0.56	45.3
East:	Mooringe	Ave									
4	L2	394	2.0	0.217	5.6	LOS A	0.0	0.0	0.00	0.57	54.7
5	T1	3	0.0	0.217	0.0	LOS A	0.0	0.0	0.00	0.57	55.9
Appro	ach	397	2.0	0.217	5.6	NA	0.0	0.0	0.00	0.57	54.7
West:	Mooringe	Ave									
11	T1	521	2.0	0.272	0.0	LOS A	0.0	0.2	0.01	0.00	60.0
12	R2	2	0.0	0.272	7.5	LOS A	0.0	0.2	0.01	0.00	57.7
Appro	ach	523	2.0	0.272	0.0	NA	0.0	0.2	0.01	0.00	60.0
All Ve	hicles	958	1.9	0.272	2.6	NA	0.2	1.3	0.00	0.26	57.0

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

LANE SUMMARY

V Site: [Mooringe Ave & New development AM]

Giveway / Yield (Two-Way)

Lane Use a	and Per	forma	ance										
		nand lows	Cap.	Deg. Satn	Lane Util.	Average Delay	Level of Service	95% Back o	f Queue	Lane Config	Lane Length		Prob. Block.
	Total	ΗV						Veh	Dist				
	veh/h	%	veh/h	v/c	%	sec			m		m	%	%
South: Acces	ss point 1												
Lane 1	38	0.0	679	0.056	100	7.7	LOS A	0.2	1.3	Full	500	0.0	0.0
Approach	38	0.0		0.056		7.7	LOS A	0.2	1.3				
East: Moorin	nge Ave												
Lane 1	397	2.0	1832	0.217	100	5.6	LOS A	0.0	0.0	Full	750	0.0	0.0
Approach	397	2.0		0.217		5.6	NA	0.0	0.0				
West: Mooring	nge Ave												
Lane 1	523	2.0	1920	0.272	100	0.0	LOS A	0.0	0.2	Full	500	0.0	0.0
Approach	523	2.0		0.272		0.0	NA	0.0	0.2				
Intersectio n	958	1.9		0.272		2.6	NA	0.2	1.3				

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Lane LOS values are based on average delay per lane.

Minor Road Approach LOS values are based on average delay for all lanes.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road lanes.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

LANE FLOWS

∇ Site: [Mooringe Ave & New development AM]

Giveway / Yield (Two-Way)

		-							
Approac			s (veh/	n)					
South: Acc		int 1							
Mov.	L2	R2	Total	%HV		Deg.	Lane	Prob.	Ov.
From S					Cap.	Satn		SL Ov.	Lane
To Exit:	W	E			veh/h	v/c	%	%	No.
Lane 1	6	32	38	0.0	679	0.056	100	NA	NA
Approac	6	32	38	0.0		0.056			
h	Ũ			0.0		0.000			
East: Moo	-								
Mov.	L2	T1	Total	%HV		Deg.		Prob.	Ov.
From E					Cap. veh/h	Satn		SL Ov.	Lane
To Exit:	S	W			ven/n	v/c	%	%	No.
Lane 1	394	3	397	2.0	1832	0.217	100	NA	NA
Approac	394	3	397	2.0		0.217			
h									
West: Moo	-								
Mov.	T1	R2	Total	%HV	0	Deg.		Prob.	Ov.
From W					Cap. veh/h	Satn v/c	Util. %	SL Ov. %	Lane No.
To Exit:	E	S			VEII/II	٧/٥	70	70	INU.
Lane 1	521	2	523	2.0	1920	0.272	100	NA	NA
Approac	521	2	523	2.0		0.272			
h									
	T ()	0(11) (5							
	Total	%HV E	Jeg.Sat	:n (v/c)					
Intersec									
tion	958	1.9		0.272					
uon									

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.

LANE LEVEL OF SERVICE

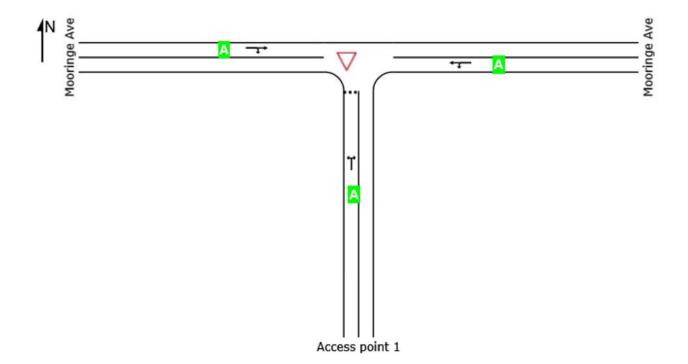
Lane Level of Service

abla Site: [Mooringe Ave & New development AM]

Giveway / Yield (Two-Way)

All Movement Classes

	South	East	West	Intersection
LOS	A	NA	NA	NA



Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Lane LOS values are based on average delay per lane.

Minor Road Approach LOS values are based on average delay for all lanes.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road lanes.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

DELAY (CONTROL)

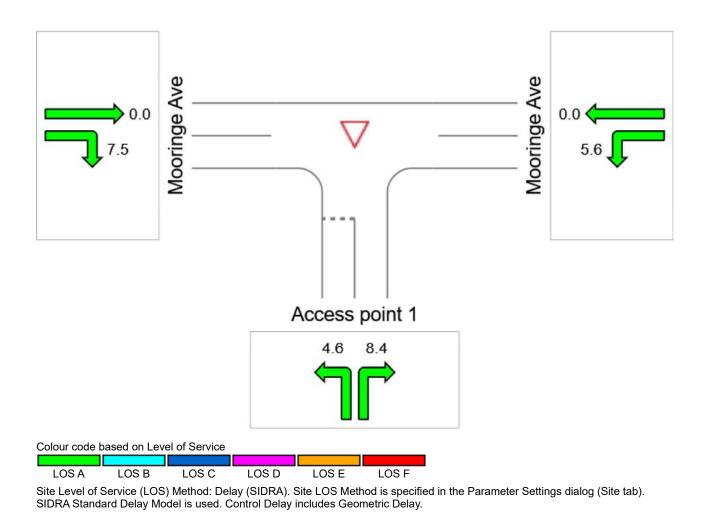
Average control delay per vehicle, or average pedestrian delay (seconds)

V Site: [Mooringe Ave & New development AM]

Giveway / Yield (Two-Way)

All Movement Classes

	South	East	West	Intersection
Delay (Control)	7.7	5.6	0.0	2.6
LOS	Α	NA	NA	NA



INTERSECTION SUMMARY

 ∇ Site: [Mooringe Ave post Pm]

Giveway / Yield (Two-Way)

Intersection Performance - Hourly Values		
Performance Measure	Vehicles	Persons
Travel Speed (Average)	57.6 km/h	57.6 km/h
Travel Distance (Total)	1089.8 veh-km/h	1307.8 pers-km/h
Travel Time (Total)	18.9 veh-h/h	22.7 pers-h/h
Demand Flows (Total)	1078 veh/h	1293 pers/h
Percent Heavy Vehicles (Demand)	2.0 %	1295 pers/fi
Degree of Saturation	0.292	
Practical Spare Capacity	180.0 %	
Effective Intersection Capacity	3693 veh/h	
Control Delay (Total)	0.64 veh-h/h	0.77 pers-h/h
Control Delay (Average)	2.1 sec	2.1 sec
Control Delay (Worst Lane)	13.6 sec 15.8 sec	15.8 sec
Control Delay (Worst Movement) Geometric Delay (Average)	1.1 sec	15.8 Sec
Stop-Line Delay (Average)	1.1 sec	
Idling Time (Average)	0.6 sec	
Intersection Level of Service (LOS)	NA	
95% Back of Queue - Vehicles (Worst Lane)	1.1 veh	
95% Back of Queue - Distance (Worst Lane)	7.7 m	
Queue Storage Ratio (Worst Lane)	0.01	
Total Effective Stops	154 veh/h	185 pers/h
Effective Stop Rate	0.14 per veh	0.14 per pers
Proportion Queued Performance Index	0.12 22.8	0.12 22.8
	22.0	22.0
Cost (Total)	430.91 \$/h	430.91 \$/h
Fuel Consumption (Total)	74.2 L/h	
Carbon Dioxide (Total)	175.4 kg/h	
Hydrocarbons (Total)	0.013 kg/h	
Carbon Monoxide (Total)	0.214 kg/h	
NOx (Total)	0.162 kg/h	

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). NA: Intersection LOS for Vehicles is Not Applicable for two-way sign control since the average intersection delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Performance Measure	Vehicles	Persons
Demand Flows (Total)	517,390 veh/y	620,867 pers/y
Delay	308 veh-h/y	370 pers-h/y
Effective Stops	74,145 veh/y	88,974 pers/y
Travel Distance	523,100 veh-km/y	627,721 pers-km/y
Travel Time	9,086 veh-h/y	10,903 pers-h/y
Cost	206,835 \$/y	206,835 \$/y
Fuel Consumption	35,594 L/y	-
Carbon Dioxide	84,177 kg/y	
Hydrocarbons	6 kg/y	
Carbon Monoxide	103 kg/y	
NOx	78 kg/y	

MOVEMENT SUMMARY

✓ Site: [Mooringe Ave post Pm]

Giveway / Yield (Two-Way)

Move	ement Pe	erformance	- Vehic	les							
Mov ID	OD Mov	Demand I Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h
South	: Streeter	s Rd (S)									
1	L2	1	0.0	0.007	7.5	LOS A	0.0	0.1	0.61	0.70	50.0
2	T1	1	0.0	0.007	10.6	LOS B	0.0	0.1	0.61	0.70	50.2
3	R2	1	0.0	0.007	13.3	LOS B	0.0	0.1	0.61	0.70	49.5
Appro	ach	3	0.0	0.007	10.5	LOS B	0.0	0.1	0.61	0.70	49.9
East:	Mooringe	Avenue (E)									
4	L2	11	2.0	0.292	7.3	LOS A	0.3	2.4	0.08	0.04	57.6
5	T1	521	2.0	0.292	0.2	LOS A	0.3	2.4	0.08	0.04	59.3
6	R2	26	2.0	0.292	7.6	LOS A	0.3	2.4	0.08	0.04	57.0
Appro	ach	558	2.0	0.292	0.6	NA	0.3	2.4	0.08	0.04	59.2
North	Streeters	s Rd (N)									
7	L2	32	2.0	0.286	7.6	LOS A	1.1	7.7	0.66	0.86	47.9
8	T1	2	0.0	0.286	12.4	LOS B	1.1	7.7	0.66	0.86	48.1
9	R2	87	2.0	0.286	15.8	LOS C	1.1	7.7	0.66	0.86	47.7
Appro	ach	121	2.0	0.286	13.6	LOS B	1.1	7.7	0.66	0.86	47.7
West:	Mooringe	e Avenue (W)									
10	L2	42	2.0	0.198	5.7	LOS A	0.0	0.3	0.01	0.07	57.6
11	T1	352	2.0	0.198	0.0	LOS A	0.0	0.3	0.01	0.07	59.3
12	R2	2	0.0	0.198	8.2	LOS A	0.0	0.3	0.01	0.07	57.3
Appro	ach	396	2.0	0.198	0.7	NA	0.0	0.3	0.01	0.07	59.1
All Ve	hicles	1078	2.0	0.292	2.1	NA	1.1	7.7	0.12	0.14	57.6

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

LANE SUMMARY

✓ Site: [Mooringe Ave post Pm]

Giveway / Yield (Two-Way)

Lane Use a	nd Perf	forma	ince										
		nand Iows	Cap.	Deg. Satn	Lane Util.	Average Delay	Level of Service	95% Back of	Queue	Lane Config	Lane Length		Prob. Block.
	Total	HV						Veh	Dist				
0 11 01	veh/h	%	veh/h	v/c	%	sec			m		m	%	%
South: Street	ters Rd (S)											
Lane 1	3	0.0	482	0.007	100	10.5	LOS B	0.0	0.1	Full	500	0.0	0.0
Approach	3	0.0		0.007		10.5	LOS B	0.0	0.1				
East: Mooring	ge Aveni	ue (E)											
Lane 1	558	2.0	1911	0.292	100	0.6	LOS A	0.3	2.4	Full	500	0.0	0.0
Approach	558	2.0		0.292		0.6	NA	0.3	2.4				
North: Street	ers Rd (l	N)											
Lane 1	121	2.0	424	0.286	100	13.6	LOS B	1.1	7.7	Full	500	0.0	0.0
Approach	121	2.0		0.286		13.6	LOS B	1.1	7.7				
West: Moorin	ige Aven	ue (N	/)										
Lane 1	396	2.0	2004	0.198	100	0.7	LOS A	0.0	0.3	Full	500	0.0	0.0
Approach	396	2.0		0.198		0.7	NA	0.0	0.3				
Intersectio n	1078	2.0		0.292		2.1	NA	1.1	7.7				

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Lane LOS values are based on average delay per lane.

Minor Road Approach LOS values are based on average delay for all lanes.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road lanes.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

LANE FLOWS

 ∇ Site: [Mooringe Ave post Pm]

Giveway / Yield (Two-Way)

Approac			s (veh/	h)							
South: Str		. ,									
Mov.	L2	T1	R2	Total	%HV		Deg.	Lane		Ov.	
From S						Cap. veh/h	Satn v/c	Util. %	SL Ov. %	Lane No.	
To Exit:	W	Ν	E			VCH/H	V/C	70	70	INU.	
Lane 1	1	1	1	3	0.0	482	0.007	100	NA	NA	
Approac	1	1	1	3	0.0		0.007				
h											
East: Moo	oringe Av	venue (I	E)								
Mov.	L2	T1	R2	Total	%HV		Deg.	Lane	Prob.	Ov.	
From E						Cap.	Satn		SL Ov.	Lane	
To Exit:	S	W	Ν			veh/h	v/c	%	%	No.	
Lane 1	11	521	26	558	2.0	1911	0.292	100	NA	NA	
Approac	11	521	26	558	2.0		0.292				
h											
North: Str	eeters F	Rd (N)									
Mov.	L2	T1	R2	Total	%HV		Deg.		Prob.	Ov.	
From N						Cap.	Satn		SL Ov.	Lane	
To Exit:	E	S	W			veh/h	v/c	%	%	No.	
Lane 1	32	2	87	121	2.0	424	0.286	100	NA	NA	
Approac	32	2	87	121	2.0		0.286				
h											
West: Mo	oringe A	venue (W)								
Mov.	L2	T1	R2	Total	%HV		Deg.	Lane	Prob.	Ov.	
From W						Cap.	Satn	Util.	SL Ov.	Lane	
To Exit:	Ν	Е	S			veh/h	v/c	%	%	No.	
Lane 1	42	352	2	396	2.0	2004	0.198	100	NA	NA	
Approac	42	352	2	396	2.0		0.198				
h											
	Total	%HV D	Deg.Sat	n (v/c)							
Intersec	4070										
tion	1078	2.0		0.292							
uon											

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.

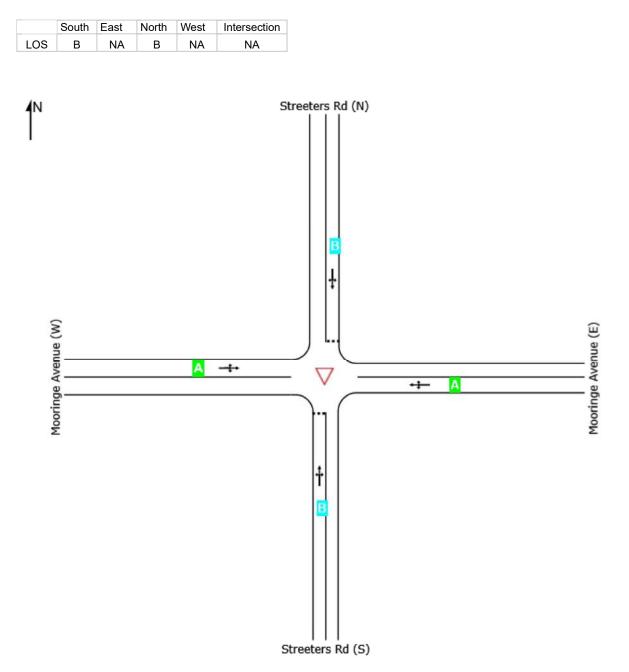
LANE LEVEL OF SERVICE

Lane Level of Service

✓ Site: [Mooringe Ave post Pm]

Giveway / Yield (Two-Way)

All Movement Classes



Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Lane LOS values are based on average delay per lane.

Minor Road Approach LOS values are based on average delay for all lanes.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road lanes.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Project: V:\2019\190100 - 190199\190190 - Mooringe Ave\Design\Calculations\Traffic\SIDRA\190190-CA-TT-A-0001[B].sip7

DELAY (CONTROL)

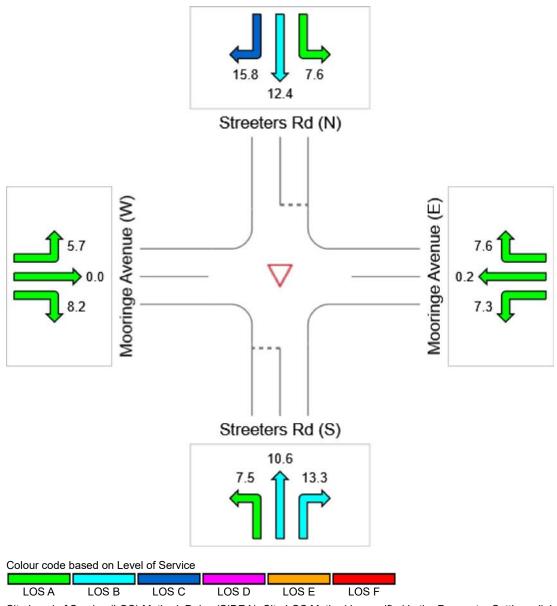
Average control delay per vehicle, or average pedestrian delay (seconds)

✓ Site: [Mooringe Ave post Pm]

Giveway / Yield (Two-Way)

All Movement Classes

	South	East	North	West	Intersection
Delay (Control)	10.5	0.6	13.6	0.7	2.1
LOS	В	NA	В	NA	NA



Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

INTERSECTION SUMMARY

✓ Site: [Mooringe Ave & New development PM]

Giveway / Yield (Two-Way)

Intersection Performance - Hourly Values		
Performance Measure	Vehicles	Persons
Travel Speed (Average) Travel Distance (Total) Travel Time (Total)	56.6 km/h 1187.0 veh-km/h 21.0 veh-h/h	56.6 km/h 1424.4 pers-km/h 25.2 pers-h/h
Demand Flows (Total) Percent Heavy Vehicles (Demand) Degree of Saturation Practical Spare Capacity Effective Intersection Capacity	941 veh/h 1.9 % 0.315 211.0 % 2986 veh/h	1129 pers/h
Control Delay (Total) Control Delay (Average) Control Delay (Worst Lane) Control Delay (Worst Movement) Geometric Delay (Average) Stop-Line Delay (Average) Idling Time (Average) Intersection Level of Service (LOS)	0.89 veh-h/h 3.4 sec 6.8 sec 8.5 sec 3.3 sec 0.1 sec 0.0 sec NA	1.06 pers-h/h 3.4 sec 8.5 sec
95% Back of Queue - Vehicles (Worst Lane) 95% Back of Queue - Distance (Worst Lane) Queue Storage Ratio (Worst Lane) Total Effective Stops Effective Stop Rate Proportion Queued Performance Index	0.1 veh 0.6 m 0.00 322 veh/h 0.34 per veh 0.01 22.6	387 pers/h 0.34 per pers 0.01 22.6
Cost (Total) Fuel Consumption (Total) Carbon Dioxide (Total) Hydrocarbons (Total) Carbon Monoxide (Total) NOx (Total)	522.70 \$/h 87.7 L/h 207.3 kg/h 0.016 kg/h 0.247 kg/h 0.205 kg/h	522.70 \$/h

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). NA: Intersection LOS for Vehicles is Not Applicable for two-way sign control since the average intersection delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Performance Measure	Vehicles	Persons
Demand Flows (Total)	451,705 veh/y	542,046 pers/y
Delay	426 veh-h/y	511 pers-h/y
Effective Stops	154,798 veh/y	185,758 pers/y
Travel Distance	569,767 veh-km/y	683,721 pers-km/y
Travel Time	10,065 veh-h/y	12,078 pers-h/y
Cost	250,894 \$/y	250,894 \$/y
Fuel Consumption	42,104 L/y	-
Carbon Dioxide	99,503 kg/y	
Hydrocarbons	8 kg/y	
Carbon Monoxide	118 kg/y	
NOx	99 kg/y	

MOVEMENT SUMMARY

V Site: [Mooringe Ave & New development PM]

Giveway / Yield (Two-Way)

Move	ement Pe	rformance	- Vehic	les							
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h
South	: Access p	oint 1									
1	L2	1	0.0	0.005	4.6	LOS A	0.0	0.1	0.14	0.56	45.3
3	R2	3	0.0	0.005	7.5	LOS A	0.0	0.1	0.14	0.56	45.8
Appro	ach	4	0.0	0.005	6.8	LOS A	0.0	0.1	0.14	0.56	45.7
East:	Mooringe	Ave									
4	L2	547	2.0	0.315	5.6	LOS A	0.0	0.0	0.00	0.55	54.9
5	T1	32	0.0	0.315	0.1	LOS A	0.0	0.0	0.00	0.55	56.1
Appro	ach	579	1.9	0.315	5.3	NA	0.0	0.0	0.00	0.55	54.9
West:	Mooringe	Ave									
11	T1	352	2.0	0.189	0.1	LOS A	0.1	0.6	0.03	0.01	59.8
12	R2	6	0.0	0.189	8.5	LOS A	0.1	0.6	0.03	0.01	57.5
Appro	ach	358	2.0	0.189	0.2	NA	0.1	0.6	0.03	0.01	59.8
All Ve	hicles	941	1.9	0.315	3.4	NA	0.1	0.6	0.01	0.34	56.6

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

LANE SUMMARY

V Site: [Mooringe Ave & New development PM]

Giveway / Yield (Two-Way)

Lane Use a	and Perf	forma	ance										
		nand lows	Cap.	Deg. Satn	Lane Util.	Average Delay	Level of Service	95% Back o	f Queue	Lane Config	Lane Length		Prob. Block.
	Total	ΗV						Veh	Dist				
	veh/h	%	veh/h	v/c	%	sec			m		m	%	%
South: Acces	ss point 1	1											
Lane 1	4	0.0	789	0.005	100	6.8	LOS A	0.0	0.1	Full	500	0.0	0.0
Approach	4	0.0		0.005		6.8	LOS A	0.0	0.1				
East: Moorin	ige Ave												
Lane 1	579	1.9	1837	0.315	100	5.3	LOS A	0.0	0.0	Full	750	0.0	0.0
Approach	579	1.9		0.315		5.3	NA	0.0	0.0				
West: Mooring	nge Ave												
Lane 1	358	2.0	1892	0.189	100	0.2	LOS A	0.1	0.6	Full	500	0.0	0.0
Approach	358	2.0		0.189		0.2	NA	0.1	0.6				
Intersectio n	941	1.9		0.315		3.4	NA	0.1	0.6				

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Lane LOS values are based on average delay per lane.

Minor Road Approach LOS values are based on average delay for all lanes.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road lanes.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

LANE FLOWS

∇ Site: [Mooringe Ave & New development PM]

Giveway / Yield (Two-Way)

A			. / I _/	I- \					
Approac			s (ven/	n)					
South: Acc	· ·								
Mov.	L2	R2	Total	%HV	<u> </u>	Deg.	Lane	Prob.	Ov.
From S					Cap. veh/h	Satn		SL Ov.	Lane
To Exit:	W	E			ven/n	v/c	%	%	No.
Lane 1	1	3	4	0.0	789	0.005	100	NA	NA
Approac	1	3	4	0.0		0.005			
h									
East Mars									
East: Moo	•		T 1 4	0/111					
Mov.	L2	T1	Total	%HV	 	Deg.	Lane	Prob. SL Ov.	Ov.
From E					Cap. veh/h	Satn v/c	0tii. %	SL OV. %	Lane No.
To Exit:	S	W							
Lane 1	547	32	579	1.9	1837	0.315	100	NA	NA
Approac	547	32	579	1.9		0.315			
h									
West: Mod	oringe A								
Mov.	T1	R2	Total	%HV		Dog	Lono	Prob.	Ov.
		R2	Total	70 ⊓ V	Cap.	Deg. Satn	Lane	SL Ov.	Lane
From W To Exit:	Е	S			veh/h	V/C	%	% %	No.
Lane 1	352	6	358	2.0	1892	0.189	100	NA	NA
Approac	352	6	358	2.0		0.189			
h									
	Total	%HV [Ded Sat	n (v/c)					
		/		(1, 0)					
Intersec	941	1.9		0.315					
tion	041	1.0		0.010					

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.

LANE LEVEL OF SERVICE

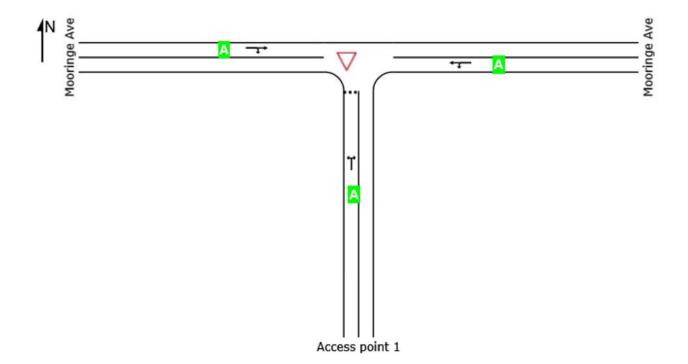
Lane Level of Service

abla Site: [Mooringe Ave & New development PM]

Giveway / Yield (Two-Way)

All Movement Classes

	South	East	West	Intersection
LOS	Α	NA	NA	NA



Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Lane LOS values are based on average delay per lane.

Minor Road Approach LOS values are based on average delay for all lanes.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road lanes.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

DELAY (CONTROL)

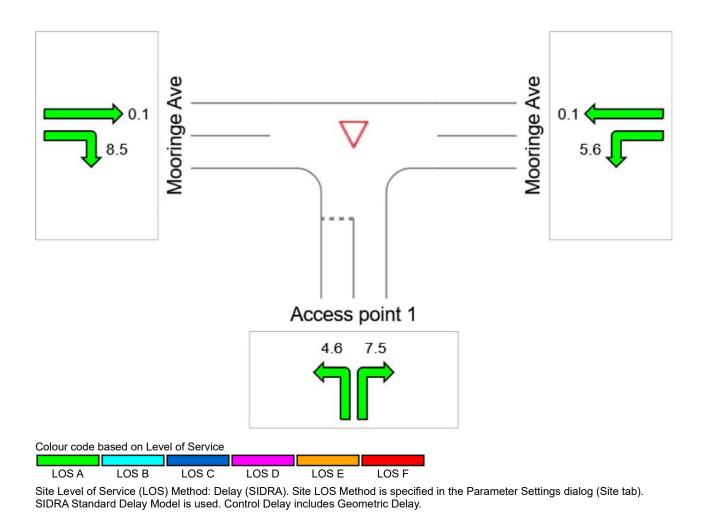
Average control delay per vehicle, or average pedestrian delay (seconds)

V Site: [Mooringe Ave & New development PM]

Giveway / Yield (Two-Way)

All Movement Classes

	South	East	West	Intersection
Delay (Control)	6.8	5.3	0.2	3.4
LOS	Α	NA	NA	NA



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Project: V:\2019\190100 - 190199\190190 - Mooringe Ave\Design\Calculations\Traffic\SIDRA\190190-CA-TT-A-0001[B].sip7

INTERSECTION SUMMARY

Site: [Mooringe & marion Rd Future Am]

Three-way intersection with "Seagull" treatment (Signals)

Signals - Fixed Time Isolated Cycle Time = 120 seconds (User-Given Cycle Time)

Variable Sequence Analysis applied. The results are given for the selected output sequence.

Intersection Performance - Hourly Values		
Performance Measure	Vehicles	Persons
Travel Speed (Average) Travel Distance (Total) Travel Time (Total)	34.1 km/h 2538.7 veh-km/h 74.4 veh-h/h	34.1 km/h 3046.4 pers-km/h 89.3 pers-h/h
Demand Flows (Total) Percent Heavy Vehicles (Demand) Degree of Saturation Practical Spare Capacity Effective Intersection Capacity	3561 veh/h 4.9 % 0.869 3.5 % 4096 veh/h	4273 pers/h
Control Delay (Total) Control Delay (Average) Control Delay (Worst Lane) Control Delay (Worst Movement) Geometric Delay (Average) Stop-Line Delay (Average) Idling Time (Average)	31.49 veh-h/h 31.8 sec 64.9 sec 64.9 sec 1.8 sec 30.1 sec 26.1 sec	37.78 pers-h/h 31.8 sec 64.9 sec
Intersection Level of Service (LOS)	LOS C	
95% Back of Queue - Vehicles (Worst Lane) 95% Back of Queue - Distance (Worst Lane) Queue Storage Ratio (Worst Lane) Total Effective Stops Effective Stop Rate Proportion Queued Performance Index	45.7 veh 329.5 m 1.05 2763 veh/h 0.78 per veh 0.80 281.5	3316 pers/h 0.78 per pers 0.80 281.5
Cost (Total) Fuel Consumption (Total) Carbon Dioxide (Total) Hydrocarbons (Total) Carbon Monoxide (Total) NOx (Total)	2393.76 \$/h 313.8 L/h 746.1 kg/h 0.068 kg/h 0.786 kg/h 1.565 kg/h	2393.76 \$/h

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Intersection LOS value for Vehicles is based on average delay for all vehicle movements. SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Performance Measure	Vehicles	Persons
Demand Flows (Total)	1,709,305 veh/y	2,051,167 pers/y
Delay	15,113 veh-h/y	18,135 pers-h/y
Effective Stops	1,326,271 veh/y	1,591,525 pers/y
Travel Distance	1,218,563 veh-km/y	1,462,276 pers-km/y
Travel Time	35,733 veh-h/y	42,879 pers-h/y
Cost	1,149,002 \$/y	1,149,002 \$/y
Fuel Consumption	150,638 L/y	
Carbon Dioxide	358,150 kg/y	
Hydrocarbons	33 kg/y	
Carbon Monoxide	377 kg/y	
NOx	751 kg/y	

MOVEMENT SUMMARY

Site: [Mooringe & marion Rd Future Am]

Three-way intersection with "Seagull" treatment (Signals)

Signals - Fixed Time Isolated Cycle Time = 120 seconds (User-Given Cycle Time)

Variable Sequence Analysis applied. The results are given for the selected output sequence.

Move	Movement Performance - Vehicles											
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h	
South	South: Marion Rd (S)											
4	L2	105	6.0	0.853	37.2	LOS D	45.7	329.5	0.95	0.91	33.2	
5	T1	1554	3.2	0.853	31.9	LOS C	45.7	329.5	0.95	0.91	32.6	
Appro	ach	1659	3.4	0.853	32.2	LOS C	45.7	329.5	0.95	0.91	32.7	
North	North: Marion Rd (N)											
11	T1	899	5.0	0.331	5.9	LOS A	9.1	66.5	0.38	0.34	52.0	
12	R2	277	10.3	0.691	53.3	LOS D	14.3	108.8	0.97	1.02	30.4	
Appro	bach	1176	6.3	0.691	17.1	LOS B	14.3	108.8	0.52	0.50	42.5	
West:	Mooringe	Ave (W)										
1	L2	481	6.1	0.869	49.6	LOS D	27.8	204.9	0.90	0.92	31.5	
3	R2	245	6.9	0.831	64.9	LOS E	15.3	113.8	1.00	0.92	23.2	
Appro	ach	726	6.4	0.869	54.8	LOS D	27.8	204.9	0.93	0.92	28.7	
All Ve	hicles	3561	4.9	0.869	31.8	LOS C	45.7	329.5	0.80	0.78	34.1	

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

LANE SUMMARY

Site: [Mooringe & marion Rd Future Am]

Three-way intersection with "Seagull" treatment (Signals)

Signals - Fixed Time Isolated Cycle Time = 120 seconds (User-Given Cycle Time)

Variable Sequence Analysis applied. The results are given for the selected output sequence.

Lane Use a	Lane Use and Performance												
	Dema Flo		Cap.	Deg. Satn	Lane Util.	Average Delay	Level of Service	95% Back o	f Queue	Lane Config	Lane Length		Prob. Block.
	Total veh/h	HV %	veh/h	v/c	%	sec		Veh	Dist m		m	, %	%
South: Mario			VGII/II	V/C	/0	360				_		/0	/0
Lane 1	850	3.5	996	0.853	100	32.2	LOS C	45.7	329.5	Full	192	0.0	<mark>54.7</mark>
Lane 2	809	3.2	948	0.853	100	32.2	LOS C	44.0	316.2	Full	192	0.0	<mark>50.9</mark>
Approach	1659	3.4		0.853		32.2	LOS C	45.7	329.5				
North: Marior	n Rd (N)												
Lane 1	452	5.0	1363	0.331	100	5.9	LOS A	9.1	66.5	Full	433	0.0	0.0
Lane 2	447	5.0	1349	0.331	100	5.9	LOS A	9.0	65.8	Full	433	0.0	0.0
Lane 3	277	10.3	401	0.691	100	53.3	LOS D	14.3	108.8	Short	130	0.0	NA
Approach	1176	6.3		0.691		17.1	LOS B	14.3	108.8				
West: Moorin	ige Ave	(W)											
Lane 1	481	6.1	553 ¹	0.869	100	49.6	LOS D	27.8	204.9	Short	70	0.0	NA
Lane 2	245	6.9	295	0.831	100	64.9	LOS E	15.3	113.8	Full	500	0.0	0.0
Approach	726	6.4		0.869		54.8	LOS D	27.8	204.9				
Intersectio n	3561	4.9		0.869		31.8	LOS C	45.7	329.5				

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Lane LOS values are based on average delay per lane.

Intersection and Approach LOS values are based on average delay for all lanes.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

1 Reduced capacity due to a short lane effect. Short lane queues may extend into the full-length lanes. Some upstream delays at entry to short lanes are not included.

LANE FLOWS

Site: [Mooringe & marion Rd Future Am]

Three-way intersection with "Seagull" treatment (Signals)

Signals - Fixed Time Isolated Cycle Time = 120 seconds (User-Given Cycle Time)

Variable Sequence Analysis applied. The results are given for the selected output sequence.

Approac	h Lane	Flows	s (veh/	h)					
South: Ma	arion Rd	l (S)							
Mov.	L2	T1	Total	%HV		Deg.		Prob.	Ov.
From S					Cap.			SL Ov.	Lane
To Exit:	W	N			veh/h	v/c	%	%	No.
Lane 1	105	745	850	3.5	996	0.853	100	NA	NA
Lane 2	-	809	809	3.2	948	0.853	100	NA	NA
Approac	105	1554	1659	3.4		0.853			
h									
North: Ma	rion Dd	(NI)							
North: Ma Mov.	non Ra T1	(N) R2	Total	%HV	_	Dec	Lone	Prob.	Ov.
	11	R2	Total	% ⊟ V	Cap.	Deg. Satn		SL OV.	Lane
From N To Exit:	S	W			veh/h	v/c	%	%	No.
Lane 1	452	-	452	5.0	1262	0.331	100	NA	NA
Lane 1	432 447		452 447	5.0	1303		100	NA	NA
		- 277	447 277			0.551	100	0.0	NA 2
Lane 3 Approac	-			10.3	401		100	0.0	2
h	899	277	1176	6.3		0.691			
11									
West: Mo	oringe A	we (W)							
Mov.	L2	R2	Total	%HV		Deg.		Prob.	Ov.
From W					Cap.	Satn		SL Ov.	Lane
To Exit:	Ν	S			veh/h	v/c	%	%	No.
Lane 1	481	-	481	6.1	553 ¹	0.869	100	<mark>100.0</mark>	2
Lane 2	-	245	245	6.9	295	0.831	100	NA	NA
Approac	481	245	726	6.4		0.869			
h									
	Total	%HV [Deg.Sat	tn (v/c)					
	rotar	/0110 6							
Intersec	3561	4.9		0.869					
tion									

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.

1 Reduced capacity due to a short lane effect. Short lane queues may extend into the full-length lanes. Some upstream delays at entry to short lanes are not included.

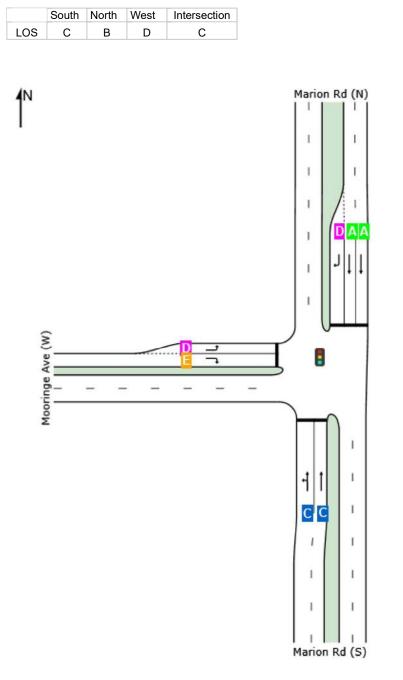
LANE LEVEL OF SERVICE

Lane Level of Service

Site: [Mooringe & marion Rd Future Am]

Three-way intersection with "Seagull" treatment (Signals) Signals - Fixed Time Isolated Cycle Time = 120 seconds (User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence.

All Movement Classes



Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Lane LOS values are based on average delay per lane.

Intersection and Approach LOS values are based on average delay for all lanes.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

DELAY (CONTROL)

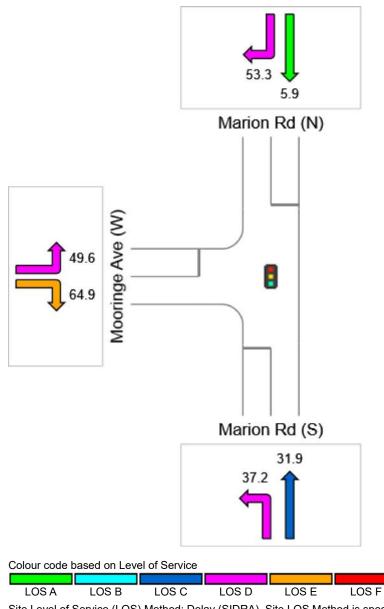
Average control delay per vehicle, or average pedestrian delay (seconds)

Site: [Mooringe & marion Rd Future Am]

Three-way intersection with "Seagull" treatment (Signals) Signals - Fixed Time Isolated Cycle Time = 120 seconds (User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence.

All Movement Classes

	South	North	West	Intersection
Delay (Control)	32.2	17.1	54.8	31.8
LOS	С	В	D	С



Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

INTERSECTION SUMMARY

Site: [Mooringe & marion Rd Future Pm]

Three-way intersection with "Seagull" treatment (Signals)

Signals - Fixed Time Isolated Cycle Time = 120 seconds (User-Given Cycle Time)

Variable Sequence Analysis applied. The results are given for the selected output sequence.

Intersection Performance - Hourly Values		
Performance Measure	Vehicles	Persons
Travel Speed (Average) Travel Distance (Total) Travel Time (Total)	37.9 km/h 2214.9 veh-km/h 58.5 veh-h/h	37.9 km/h 2657.9 pers-km/h 70.2 pers-h/h
Demand Flows (Total) Percent Heavy Vehicles (Demand) Degree of Saturation Practical Spare Capacity Effective Intersection Capacity	3165 veh/h 4.9 % 0.737 22.1 % 4295 veh/h	3798 pers/h
Control Delay (Total) Control Delay (Average) Control Delay (Worst Lane) Control Delay (Worst Movement) Geometric Delay (Average) Stop-Line Delay (Average) Idling Time (Average)	21.05 veh-h/h 23.9 sec 59.7 sec 59.7 sec 1.6 sec 22.3 sec 19.0 sec	25.26 pers-h/h 23.9 sec 59.7 sec
Intersection Level of Service (LOS)	LOS C	
95% Back of Queue - Vehicles (Worst Lane) 95% Back of Queue - Distance (Worst Lane) Queue Storage Ratio (Worst Lane) Total Effective Stops Effective Stop Rate Proportion Queued Performance Index	29.2 veh 215.8 m 0.69 2087 veh/h 0.66 per veh 0.70 199.8	2504 pers/h 0.66 per pers 0.70 199.8
Cost (Total) Fuel Consumption (Total) Carbon Dioxide (Total) Hydrocarbons (Total) Carbon Monoxide (Total) NOx (Total)	1869.76 \$/h 260.6 L/h 620.4 kg/h 0.055 kg/h 0.660 kg/h 1.378 kg/h	1869.76 \$/h

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Intersection LOS value for Vehicles is based on average delay for all vehicle movements. SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Performance Measure	Vehicles	Persons
Demand Flows (Total)	1,519,327 veh/y	1,823,192 pers/y
Delay	10,106 veh-h/y	12,127 pers-h/y
Effective Stops	1,001,571 veh/y	1,201,886 pers/y
Travel Distance	1,063,145 veh-km/y	1,275,774 pers-km/y
Travel Time	28,078 veh-h/y	33,694 pers-h/y
Cost	897,484 \$/y	897,484 \$/y
Fuel Consumption	125,081 L/y	-
Carbon Dioxide	297,793 kg/y	
Hydrocarbons	26 kg/y	
Carbon Monoxide	317 kg/y	
NOx	661 kg/y	

MOVEMENT SUMMARY

Site: [Mooringe & marion Rd Future Pm]

Three-way intersection with "Seagull" treatment (Signals)

Signals - Fixed Time Isolated Cycle Time = 120 seconds (User-Given Cycle Time)

Variable Sequence Analysis applied. The results are given for the selected output sequence.

Move	ement Pe	rformance	- Vehic	les								
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h	
South	South: Marion Rd (S)											
4	L2	165	10.8	0.719	34.9	LOS C	29.2	215.8	0.88	0.81	33.8	
5	T1	1044	5.0	0.719	29.3	LOS C	29.2	215.8	0.88	0.80	33.8	
Approach		1209	5.8	0.719	30.0	LOS C	29.2	215.8	0.88	0.80	33.8	
North	: Marion R	d (N)										
11	T1	1212	2.1	0.438	6.6	LOS A	13.7	97.7	0.43	0.39	51.2	
12	R2	302	9.4	0.557	40.4	LOS D	13.8	104.6	0.89	0.96	34.3	
Appro	bach	1514	3.5	0.557	13.4	LOS B	13.8	104.6	0.52	0.50	45.2	
West	Mooringe	Ave (W)										
1	L2	220	10.0	0.287	27.2	LOS C	7.9	60.4	0.66	0.76	39.6	
3	R2	222	3.8	0.737	59.7	LOS E	13.0	93.9	1.00	0.86	24.5	
Appro	bach	442	6.9	0.737	43.6	LOS D	13.0	93.9	0.83	0.81	31.3	
All Ve	hicles	3165	4.9	0.737	23.9	LOS C	29.2	215.8	0.70	0.66	37.9	

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

LANE SUMMARY

Site: [Mooringe & marion Rd Future Pm]

Three-way intersection with "Seagull" treatment (Signals)

Signals - Fixed Time Isolated Cycle Time = 120 seconds (User-Given Cycle Time)

Variable Sequence Analysis applied. The results are given for the selected output sequence.

Lane Use and Performance													
	Demand Flows		Cap.	Deg. Satn	Lane Util.	Average Delay	Level of Service	95% Back of Queu		e Lane Config	Lane Length		Prob. Block.
	Total	HV		Caur		Delay		Veh	Dist	Coning	Longin	Auj.	
	veh/h	%	veh/h	v/c	%	sec			m		m	%	%
South: Marion Rd (S)													
Lane 1	615	6.6	855	0.719	100	30.8	LOS C	29.2	215.8	Full	192	0.0	<mark>15.6</mark>
Lane 2	595	5.0	827	0.719	100	29.3	LOS C	28.3	206.4	Full	192	0.0	<mark>11.5</mark>
Approach	1209	5.8		0.719		30.0	LOS C	29.2	215.8				
North: Marion Rd (N)													
Lane 1	609	2.1	1389	0.438	100	6.6	LOS A	13.7	97.7	Full	433	0.0	0.0
Lane 2	603	2.1	1374	0.438	100	6.6	LOS A	13.6	96.6	Full	433	0.0	0.0
Lane 3	302	9.4	543	0.557	100	40.4	LOS D	13.8	104.6	Short	130	0.0	NA
Approach	1514	3.5		0.557		13.4	LOS B	13.8	104.6				
West: Mooringe Ave (W)													
Lane 1	220	10.0	765	0.287	100	27.2	LOS C	7.9	60.4	Short	70	0.0	NA
Lane 2	222	3.8	301	0.737	100	59.7	LOS E	13.0	93.9	Full	500	0.0	0.0
Approach	442	6.9		0.737		43.6	LOS D	13.0	93.9				
Intersectio n	3165	4.9		0.737		23.9	LOS C	29.2	215.8				

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Lane LOS values are based on average delay per lane.

Intersection and Approach LOS values are based on average delay for all lanes.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

LANE FLOWS

Site: [Mooringe & marion Rd Future Pm]

Three-way intersection with "Seagull" treatment (Signals)

Signals - Fixed Time Isolated Cycle Time = 120 seconds (User-Given Cycle Time)

Variable Sequence Analysis applied. The results are given for the selected output sequence.

Approac	Approach Lane Flows (veh/h)									
South: Ma	arion Rd	l (S)								
Mov.	L2	T1	Total	%HV		Deg.		Prob.	Ov.	
From S					Cap.	Satn		SL Ov.	Lane	
To Exit:	W	N			veh/h	v/c	%	%	No.	
Lane 1	165	450	615	6.6	855	0.719	100	NA	NA	
Lane 2	-	595	595	5.0	827	0.719	100	NA	NA	
Approac	165	1044	1209	5.8		0.719				
h										
North: Mc	rion Dd	(NI)								
North: Ma	T1	. ,	Total	%HV	_	Dec	Long	Droh	Ov.	
Mov.	11	R2	Total	%HV	Cap.	Deg. Satn		Prob. SL Ov.	Lane	
From N To Exit:	S	W			veh/h	v/c	%	%	No.	
Lane 1	609		609	2.1	1200	0.438	100	NA	NA	
		-								
Lane 2	603	-	603	2.1		0.438	100	NA	NA	
Lane 3	-	302	302	9.4	543	0.557	100	0.0	2	
Approac	1212	302	1514	3.5		0.557				
h										
West: Mo	oringe A	we (W)								
Mov.	L2	R2	Total	%HV		Deg.	Lane	Prob.	Ov.	
From W					Cap.	Satn		SL Ov.	Lane	
To Exit:	N	S			veh/h	v/c	%	%	No.	
Lane 1	220	-	220	10.0	765	0.287	100	0.0	2	
Lane 2	-	222	222	3.8	301	0.737	100	NA	NA	
Approac	220	222	442	6.9		0.737				
h										
	Total	0/11/7								
	Total	%HV [Deg.Sat	IN (V/C)						
Intersec	3165	4.9		0.737						
tion	5105	4.5		0.157						

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.

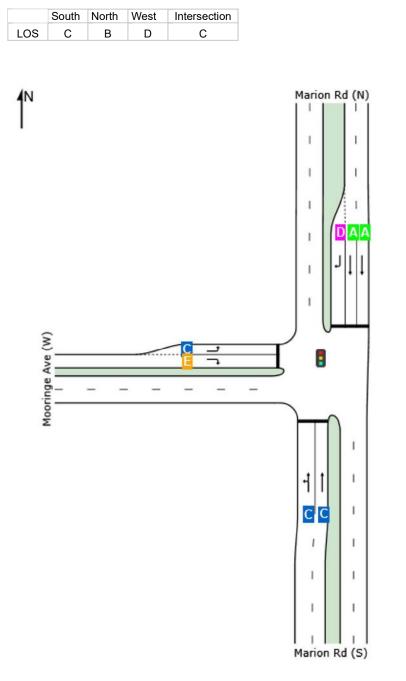
LANE LEVEL OF SERVICE

Lane Level of Service

Site: [Mooringe & marion Rd Future Pm]

Three-way intersection with "Seagull" treatment (Signals) Signals - Fixed Time Isolated Cycle Time = 120 seconds (User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence.

All Movement Classes



Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Lane LOS values are based on average delay per lane.

Intersection and Approach LOS values are based on average delay for all lanes.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

DELAY (CONTROL)

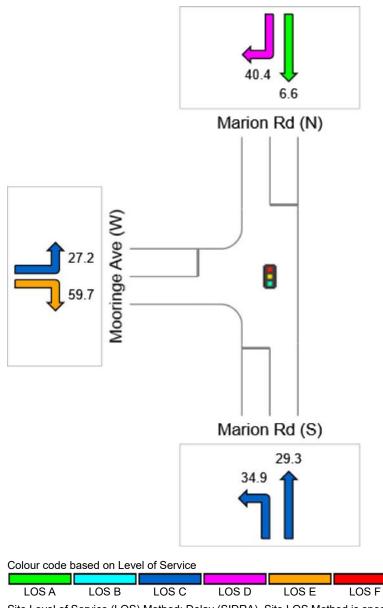
Average control delay per vehicle, or average pedestrian delay (seconds)

Site: [Mooringe & marion Rd Future Pm]

Three-way intersection with "Seagull" treatment (Signals) Signals - Fixed Time Isolated Cycle Time = 120 seconds (User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence.

All Movement Classes

	South	North	West	Intersection
Delay (Control)	30.0	13.4	43.6	23.9
LOS	С	В	D	С



Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.



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